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Dr. M.M. Bonner, Director, Advanced Systems

Abstract:

The results of a simulation study to predict the IUE imaging chain performance are presented, including simulation photographs and transparencies of ultraviolet echelle spectra. Errors in wavelength determination and radiometric measurements due to system degradation are indicated to be minor. Some order overlap is predicted at the bottom of the echelle format.

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SECTION 1

INTRODUCTION

The Perkin-Elmer Corporation Optical Technology Division in Danbury, Connecticut has performed a six month scientific study contract for the NASA/Goddard Space Flight Center, Theoretical Astrophysics Branch, Greenbelt, Maryland. (Contract No. NAS 5-23327). The study program consisted of the development of a computerized mathematical model and the production of simulated ultraviolet (UV) spectrograms on film with the aid of the Perkin-Elmer Line Scan Image Generator (LSIG). This model was used as a basis to predict the optical performance of the International Ultraviolet Explorer (IUE) Scientific Instrument which is scheduled for launch in December 1976.

The two questions of major concern in the study program were, first, the effect of the destructive readout process in the SEC vidicon camera on the accuracy of spectroradiometric data in the UV spectrogram (or "echellogram", since it is produced by crossed echelle and concave spherical gratings), and second, the question of the extent of overlap between adjacent echelle orders.

The results of the study indicate that the answer to the first question is that, to the extent that linear modeling accurately represents the imaging system, the errors in wavelength determination and radiometry introduced by destructive readout are not serious, possibly even negligible. The second question has not been completely answered. Order overlap is significant at the bottom of the echelle format where the orders are most closely spacee. Further work in the area of image enhancement, particularly desmearing in the cross-order direction, is suggested.

Section 2 discusses the development of the math model. Section 3 describes the preparation of the input echellogram computer tapes which were linearly interpolated from the NASA-furnished data. Section 4 gives the details of the simulation procedures, Section 5 discusses the results, and gives

recommendations for further work. Section 6 contains a brief summary and lists the major conclusions. Selected computer printouts of the simulation tapes are included in Appendix A, and a derivation of a series expansion formula for evaluating a Hankel integral transform is presented in Appendix B.

Positive film transparencies and photographic prints of the simulated echellograms are furnished in Volume II of this report.

SECTION 2

SYSTEM MATHEMATICAL MODEL

2.1 MODEL SUMMARY AND BLOCK DIAGRAM

A simplified functional block diagram of the International Ultraviolet Explorer (IUE) Scientific Instrument is shown in Figure 1. (A complete description of the Scientific Instrument is given in Reference 1.)

In this study program we have concerned outselves with analysis of performance degradations of only the imaging portion of the system chain extending from the telescope through the SEC vidicon camera, since effects of noise in the transmission link and reconstruction artifacts are deemed to be minor considerations relative to the questions pertaining to the discharge overlap in the SEC readout process and loss of resolution in the UV converter.

In the following paragraphs a linear analytical model suitable for computer simulation of the imaging chain effects on UV echelle spectra is developed. The destructive readout process is first discussed, and a computer algorithm for generating an "effective" point spread function (PSF) for destructive readout is presented in Paragraph 2.2. This is followed by a discussion of the derivations of the UV converter and guidance (servo jitter) transfer functions in Paragraphs 2.3 and 2.4. The echelle spectrograph is assumed to make a negligible contribution to performance degradations, as discussed in Paragraph 2.5. Cascaded transfer functions and PSF's are presented in Paragraph 2.6, and finally, a discussion of the implementation of the model on the computer is given in Paragraph 2.7. The Perkin-Elmer IBM 370/158 system was used for all the modeling computations.

2.2 DESTRUCTIVE READOUT OF SEC VIDICON

We start with the following basic assumptions concerning the destructive readout process:

a. The digitally addressed read beam current profile is circular Gaussian (although other profiles may be substituted in the model).

Figure 1. International Ultraviolet Explorer (IUE)
Scientific Instrument Functional Block Diagram

- b. The charge removed from a uniformly charged region of the SEC target during a single capacitive discharge read operation is proportional to the integral of the product of the charge density Q times the beam current profile over the spatial extent of the beam. In other words, a single read operation makes a Gaussian-shaped "hole" in the original uniform charge density (see Figure 2-b).
 - c. Target lag effects are negligible.

The linearity of the analytical model rests on the latter two assumptions.

In the following development, we first expand and generalize the one-dimensional approach outlined in some preliminary calculations done at NASA. Next, we make the important simplifying approximation which neglects the previous read operations more than a few pixels (3-4) removed from the current beam address. This approximation has the very useful result of rendering the readout integral space-invariant, which allows us to use the powerful convolution theorem for Fourier transforms. The next step is a straightforward extension to two dimensions. Finally, the discrete sum approximation to the readout integral is made, which is necessary for computer calculations.

2.2.1 One-Dimensional Readout Model

The following is depicted graphically in Figure 2 for a digitally addressed Gaussian beam profile spaced by its full-width-half-maximum (FWHM) width. The charge readout at the first beam address \mathbf{X}_1 is given by

$$M_1 = \int_{-\infty}^{\infty} QG(x-x_1)dx, \qquad (2.1)$$

where Q is the (uniform) charge density on the target, and $G(x-x_1)$ is the beam current profile, appropriately normalized, centered at x_1 (Figure 2-a). The charge density remaining at this point is clearly $Q[1-G(x-x_1)]$ (see Figure 2-b), which becomes the input to the next readout at x_2 , namely,

$$M_2 = \int_{-\infty}^{\infty} Q[1-G(x-x_1)]G(x-x_2)dx.$$
 (2.2)

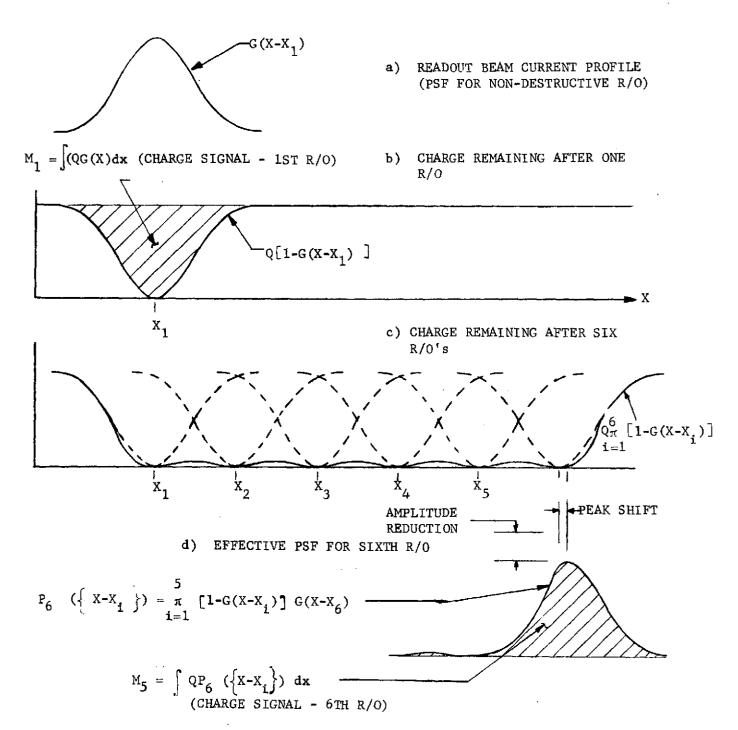


Figure 2. Destructive Readout of Uniformly Charged Target (1-dimensional Model)

Thus, at the k'th beam address, the charge readout is

$$M_{k} = \int_{-\infty}^{\infty} Q_{\pi} \left[1 - G(x - x_{1}) \right] G(x - x_{k}) dx$$
 (2.3)

2.2.2 Space-Invariant Approximation - Effective PSF

It should be apparent from the foregoing that, due to the finite extent of the readout beam, the previously read pixels more than a few addresses (3-4) removed from the current address make negligible contributions to the readout integral, Equation (2.3). For example, consider a pixel spacing of 1.5 σ , where σ is the standard deviation width of the Gaussian function $G(x) = \exp(-x^2/2\sigma^2)$. The value of G four pixels removed from the current position (x = 0 in this example) is $\exp(-18) = 1.5 \times 10^{-8}$, giving 1-G \cong 1 to one part in 10 8 .

Hence, only the 1-G factors corresponding to the nearest two or three previously read pixels need be retained in the readout integral, Equation (2.3).

Thus, we are able to make the following approximation to the readout integral, Equation (2.3):

$$M_{k} \cong \int_{-\infty}^{\infty} Q \prod_{i=k-m}^{k-1} [1-(x-x_{i})]G(x-x_{k}) dx, \qquad (2.4)$$

where we have dropped all pixel contributions more than m beam addresses removed from the current (k'th) one.

Next, we introduce the analytically convenient notion of an "effective PSF" for destructive readout by associating the product of (1-G) factors with $G(x-x_k)$, the PSF of the current readout, rather than with the charge density Q. This has the computational advantage of allowing the calculation of the destructive readout PSF, or its Fourier transform (a complex optical transfer function [OTF]), independently of the input echellogram represented by the charge distribution Q. Hence, the effective PSF for destructive readout at beam address x_k is defined by (see Figure 2-d):

$$P_{k} \left(\left\{ \mathbf{x} - \mathbf{x}_{i} \right\} \right) = \prod_{i=k-m}^{k-1} \left[1 - G(\mathbf{x} - \mathbf{x}_{i}) \right] G(\mathbf{x} - \mathbf{x}_{k}), \qquad (2.5)$$

where the braces denote the set of $x-x_i$'s over the range of the products.

If the readout lattice is of uniform spacing, which is the case for the SEC vidicon in the IUE instrument, then the G functions are independent of k, and therefore, since m is a fixed constant, the expression (2.5) is space-invariant.

Finally, we rewrite the approximation (2.5) to the readout integral, using our new definition of effective PSF, and also generalizing to the case of a variable charge density Q(x):

$$M_{k} \cong \int_{-\infty}^{\infty} Q(x) P_{k} \left(\left\{ x - x_{i} \right\} \right) dx,$$
 (2.6)

where the notation is to be understood from the definition of P in Equation (2.5). This last integral expression exhibits the form of a convolution, which, as we have already noted, is important for the purposes of computation.

2.2.3 Extension to Two Dimensions

The extension of Equations (2.5) and (2.6) to two dimensions is obvious: Q(x) goes over to Q(x,y), and the $(x-x_i)$ go over to $(x-x_i)$, $(y-y_i)$ giving

$$P_{k,\ell} (\{x-x_i\}, \{y-y_j\}) = \prod_{i,j} [1-G(x-x_i, y-y_j)]G(x-x_k, y-y_\ell)$$
 (2.7)

and

$$M_{k, \ell} \cong \int_{-\infty}^{+\infty} \int Q(x, y) P_{k, \ell} \left(\left\{ x - x_i \right\}, \left\{ y - y_i \right\} \right) dx dy$$
 (2.8)

for the two-dimensional effective PSF and charge readout expressions respectively. Since G(x,y) is circular Gaussian, it may be factored into a product of the corresponding one-dimensional functions, i.e.,

$$G(x, y) = G(x) G(y)$$

This will be convenient later on in the construction of the effective PSF computer algorithm. Note in Equation (2.7) that we have not specified the ranges of the product indices i, j. These will depend upon the particular sequence of readout beam addressing employed. In the case under study, a two-dimensional square lattice is digitally scanned in raster fashion with pixel spacings specified by NASA to be:

$$\Delta x = \Delta y = 33\mu \tag{2.9}$$

at the camera focal plane. Therefore, the beam addresses $(\mathbf{x}_{k_j}, \mathbf{y}_{\ell})$ are given by

$$\mathbf{x}_{\mathbf{k}} = \mathbf{k}\Delta\mathbf{x}$$
 , $\mathbf{k} = 0, 1, \dots, N-1$
 $\mathbf{y}_{\ell} = \ell\Delta\mathbf{y}$, $\ell = 0, 1, \dots, N-1$
(2.10)

where N is the dimension of the readout lattice. It seems most convenient to indicate the (1-G) factors retained in the product of Equation (2.7) diagrammatically, which we have done in Figure 3. Here we show the previously read pixels in the raster which are within a radius approximately $5\Delta x$ (or $5\Delta y$) of the current readout address (x_k, y_ℓ) . The numbers 1-6 indicate the degree of nearest neighbor, where 1 is the current beam position. This is helpful in keeping track of the (1-G) factors when writing the computer subroutine. The number assignments are somewhat arbitrary, but it does not matter, since the ordering of the factors in the product is immaterial. A border five pixels wide has been indicated in the diagram around three sides of the raster within which the effective PSF is not space-invariant, since (1-G) factors are progressively lost as the edges of the raster are approached (except for the left-hand side where there are no previously read pixels). However, very little information is lost by ignoring the edge regions, since they comprise a very small fraction of the total format. Moreover, the side edges are also where the blaze angle falloff of the spectrograph is greatest, so they are likely to be of little interest.

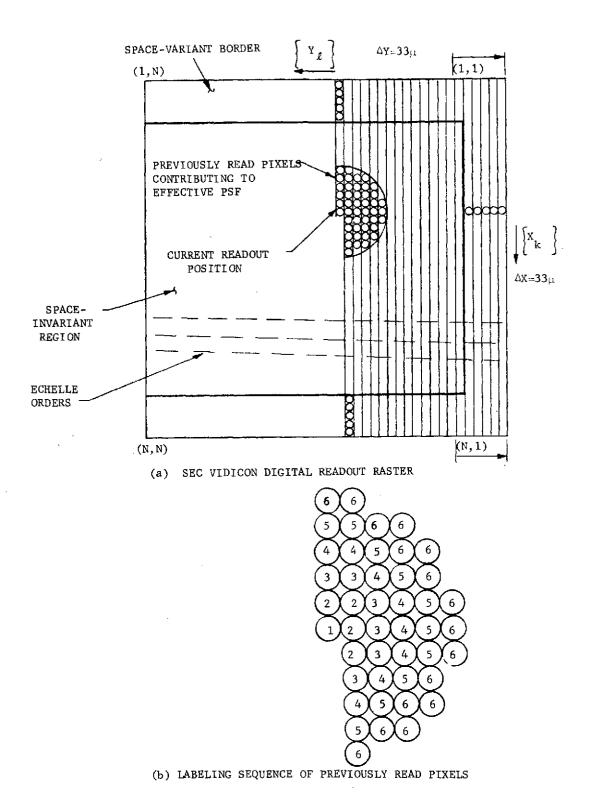


Figure 3. Readout Raster and Pixel Labeling

2.2.4 Computer Algorithm for Destructive Readout

With the aid of the labeling sequence in Figure 3-b, the (1-G) factors may readily be determined and the effective PSF constructed. In the space-invariant region, $P_{k,\ell}$ is independent of the beam address (x_k,y_ℓ) . Hence, we take the current readout position to be (0,0), also setting $k=\ell=0$. Then, the G functions for the current readout position and previously read neighboring pixels are given by (see Figure 3-b):

Programming Notation †

```
G(x)G(y) \rightarrow GXPOS(1)*GY(1) \text{ current readout position}
G(x+\Delta x)G(y) \rightarrow GXPOS(2)*GY(1)
G(x+\Delta x)G(y+\Delta y) \rightarrow GXPOS(2)GY(2)
G(x)G(y+\Delta y) \rightarrow GXPOS(1)*GY(2)
G(x-\Delta x)G(y+\Delta y) \rightarrow GXPOS(1)*GY(2)
G(x+2\Delta x)G(y) \rightarrow GXPOS(3)*GY(1)
G(x+2\Delta x)G(y) \rightarrow GXPOS(3)*GY(2)
G(x+2\Delta x)G(y+\Delta y) \rightarrow GXPOS(3)*GY(2)
second nearest neighbors
```

where the nearest, second nearest, etc. neighbors have been written in clockwise sequence, starting at the top.

From this table, the zeroth, nearest neighbor, second nearest neighbor, etc. approximations to the effective PSF may be constructed as follows:

```
Zeroth approximation (equivalent to nondestructive readout):
```

```
PSF(1) = C*GXPOS(1)*GY(1)
```

Nearest neighbor approximation:

$$PSF(2) = PSF(1)*(1 - C*GXPOS(2)*GY(1))*(1 - C*GXPOS(2)*GY(2))$$

$$*(1 - C*GXPOS(1)*GY(2))*(1 - C*GXNEG(2)*GY(2))$$

Second nearest neighbor approximation:

$$PSF(3) = PSF(2)*(1 - C*GXPOS(3)*GY(1))*(1 - C*GXPOS(3)*GY(2))$$

[†] The notations GXPOS, GXNEG refer to previously read pixels in the x>0, x<0 half-planes respectively. GY is not so distinguished since all pixels are in the y<0 half-plane.

Note that a parameter C (0 \leq C \leq 1) has been introduced which takes account of the possibility of less than 100% target discharge at the center of the readout beam.

The above construction has been carried out to the fifth nearest neighbor approximation for the circular Gaussian case, and programmed as FORTRAN subroutine SECPSF. A listing can be found in Figure 4.

2.2.5 Effective PSF Features

Subroutine SECPSF was used to make perspective plots of the effective PSF on Perkin-Elmer's Calcomp plotter for two ratios of pixel spacing-to-beam sigma width: $\Delta x/\sigma = 1.551$, and 2.35 (FWHM spacing). For comparison, the circular Gaussian (nondestructive R/O) PSF was also plotted. These are shown in Figures 5 to 7. The x- and y-axes have been labelled in units of σ . The view is from the negative x, negative y quadrant. The PSF maxima relative to unit height for the nondestructive case are indicated in the graphs. Corresponding numerical printouts of the nondestructive and destructive readout processing arrays appear in Figures 8 and 9. These arrays are calculated from subroutine SECPSF at points on the computational sampling lattice which is interpolated 2:1 from the readout lattice. (See Section 2.7 for a discussion of the requirement for interpolation.)

The most obvious features to be noticed in the perspective plots are the shift of the PSF maximum relative to the center of the beam, and the two nearest neighbor holes located on the x- and y-axes. The "ripple", or residual charge, between these holes is also visible. The scale of the plots is not large enough to see the effects of the second and higher nearest neighbors; these can be seen in the processing array printouts. PSF profiles for the case $\Delta x/\sigma = 1.551$ at constant x and at constant y are plotted in Figure 10 from the array data in Figure 8.

The shift of the maximum and the ripple effects are most evident for the $\Delta x/\sigma = 1.551$ case, which corresponds to the greatest amount of beam overlap. This value is derived from the NASA-furnished parameter values of

```
SUBROUTINE SECPSF(X,Y,DX,DY,SIG,C,KNEAR,PSF)
                   DIMENSION PSF(1), GXPOS(6), GXMEG(6), GY(6)
                   DXX=DX/SIG
                   DYY=DY/SIG
                   XX=X/SIG
                   YY=Y/SIG
                    IMAX=KNEAR+1
                   DO 1 I=1, IMAX
                   XPSHF=XX+(1-1)*DXX
                   XXPSHF=XPSHF*XPSHF/2.
                   XNSHF = XX - (I-1) *DXX
                   XXNSHF=XNSHF * XNSHF / 2.
                   YSHF=YY+(I-1)*DYY
                   YYSHF=YSHF*YSHF/2.
                    IF(XXPSHF.GT.25.)XXPSHF=25.
                    IF(XXNSHF.GT.25.)XXNSHF≈25.
                    IF(YYSHF.GT.25.)YYSHF=25.
                    IF(XXPSHF.LT.-25.)XXPSHF=-25.
                    IF(XXNSHF.LT.-25.)XXNSHF=-25.
                    IF(YYSHF.LT.-25.)YYSHF=-25.
                   GXPOS(1) = EXP(-XXPSHF)
                    GXNEG(1)=EXP(-XXNSHF)
1
                    GY(1) = EXP(-YYSHF)
                    PSF(1)=C*GXPOS(1)*GY(1)
                    IF(KNEAR.LE.O)GO TO 2
                    PSF(2)=PSF(1)*(1.-C*GXPOS(2)*GY(1))*(1.-C*GXPOS(2)*GY(2))*(1.-C*GX
                ZPOS(1)*GY(2))*(1.-C*GXNEG(2)*GY(2))
                    IF(KNEAR.EQ.1)GO TO 2
                    PSF(3)=PSF(2)*(1.-C*GXPOS(3)*GY(1))*(1.-C*GXPOS(3)*GY(2))*(1.-C*GX
                 ZPOS(2)*GY(3)
                 Z*(1.-C*GXPOS(1)*GY(3))*(1.-C*GXNEG(2)*GY(3))*(1.-C*GXNEG(3)*GY(2))
                     IF(KNEAR.EQ.2)GO TO 2
                    PSF(4) = PSF(3) * (1.-C*GXPOS(4)*GY(1))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(2))*(1.-C*GXPOS(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*GY(4)*G
                ZPOS(3)*GY(3))*(1.-C*GXPOS(2)*GY(4))
                 Z*(1.-C*GXPOS(1)*GY(4))*(1.-C*GXNEG(2)*GY(4))*(1.-C*GXNEG(3)*GY(3))
                 Z*(1.-C*GXNEG(4)*GY(2))
                     IF(KNEAR.EQ.3)GO TO 2
                    PSF(5)=PSF(4)*(1.-C*GXPOS(5)*GY(1))*(1.-C*GXPOS(5)*GY(2))*(1.-C*GX
                 ZPOS(4)*GY(3))*(1.-C*GXPOS(3)*GY(4))
                 Z*(1.~C*GXPOS(2)*GY(5))*(1.~C*GXPOS(1)*GY(5))*(1.~C*GXNEG(2)*GY(
                 Z5))*(1.~C*GXNEG(3)*GY(4))
                 Z*(1.~C*GXNEG(4)*GY(3))*(1.~C*GXNEG(5)*GY(2))
                     IF(KNEAR, EQ. 4)GO TO 2
                    PSF(6) = PSF(5)*(1.-C*GXPOS(6)*GY(1))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-C*GXPOS(G)*GY(2))*(1.-
                 ZPOS(5)*GY(3))*(1.-C*GXPOS(5)*GY(4))*(1.-C*GXPOS(4)*GY(4))
                 Z*(1.-C*GXPOS(4)*GY(5))*(1.-C*GXPOS(3)*GY(5))*(1.-C*GXPOS(2)*GY(5))
                 Z6))*(1.-C*GXPOS(1)*GY(6))
                  Z*(1.-C*GXNEG(2)*GY(6))*(1.-C*GXNEG(3)*GY(5))*(1.-C*GXNEG(4)*GY(5))
                  Z*(1.-C*GXNEG(4)*GY(4))
                  Z*(1.-C*GXNEG(5)*GY(4))*(1.-C*GXNEG(5)*GY(3))*(1.-C*GXNEG(6)*GY(2))
                     RETURN
 2
                     END
```

Figure 4. Computer Subroutine for Destructive R/O of SEC Vidicon

14:31:16

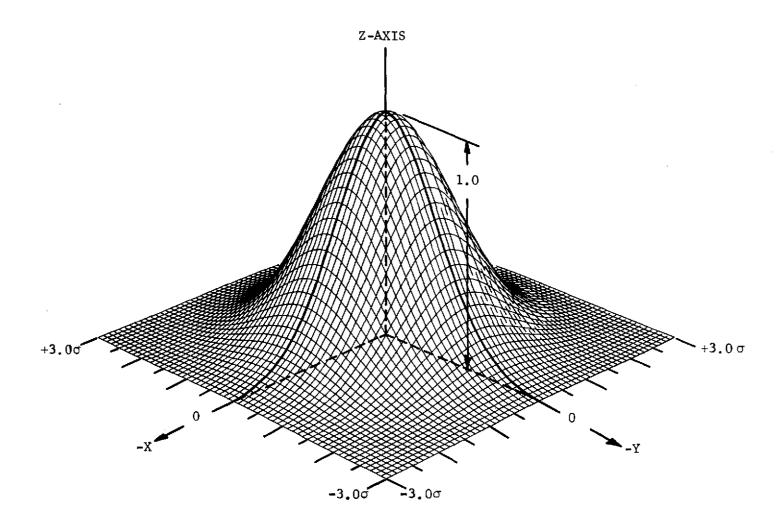


Figure 5. Gaussian Beam Current Distribution (PSF For Non-Destructive R/O)

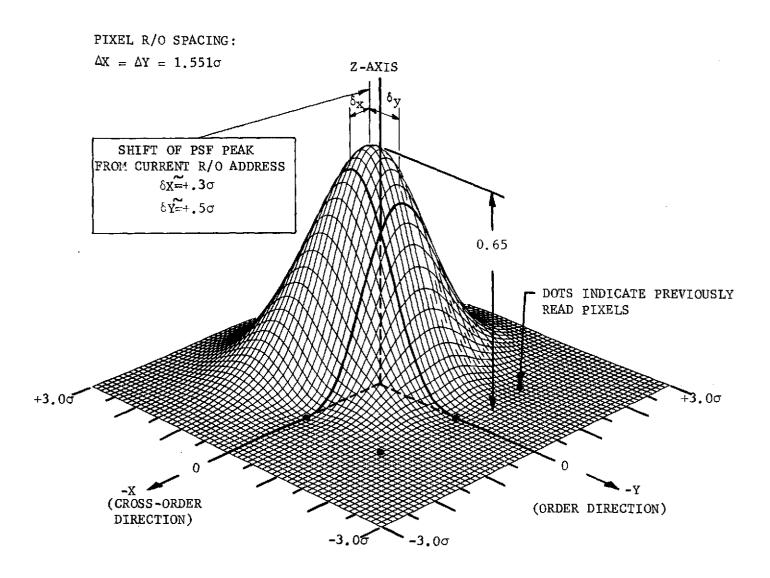


Figure 6. Effective PSF For SEC Vidicon Destructive R/O (100 Percent Discharge)

PIXEL R/O SPACING:

 $\Delta X = \Delta Y = 2.35\sigma$

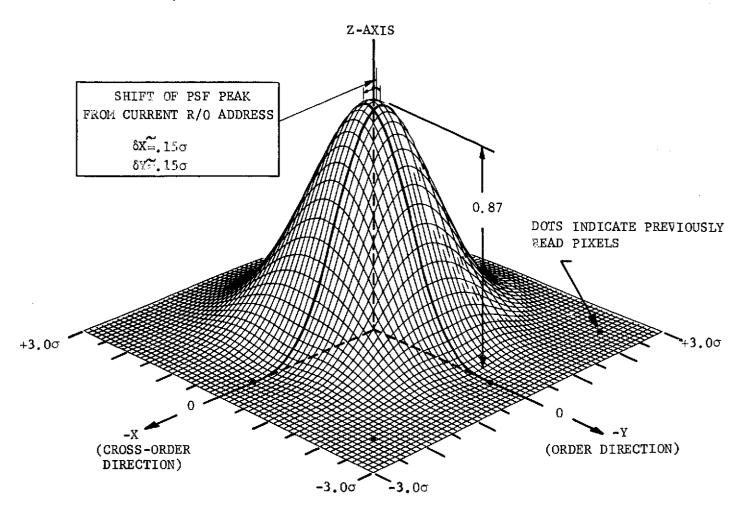


Figure 7. Effective PSF for SEC Vidicon Destructive R/O (100 Percent Discharge)

SECRSE2D TEST

DX= 16.500000 DY= 16.500000 XMIN= -99.000000 XMAX= 99.000000 YMIN= -99.000000 YMAX= 99.000000 DISCH FRACTION= 1.000000 DXSEC= 33.000000 DYSEC= 33.000000 SIG= 21.276993

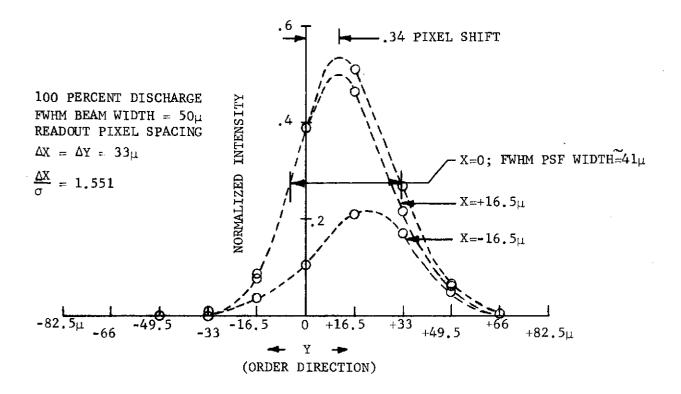
DROPSE(P(6) **→** +x 0-0000 0-0 0.0000 0.0 0.0000 0.0 0.0000 0.0 0.0 0.0000 0.0 0.0000 0.0 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0001 0.0 0.0001 0.0 0.0000 0.0 0.0000 0.0 0.0000 0.0 0.0000 0.0 0.0000 0.0000 0.0000 0.0001 0.0004 0.0014 0.0014 0.0015 0.0004 0.0001 0.0000 0.0000 0.0000 0-0007 0-0 0.0000 0.0 0-0004 0-0 0.0057 0.0 0.0073 0.0 0.0000 0.0 0.0000 0.0000 0.0001 0.0016 0.0062 0.0388 0.0794 0.0859 0.0307 0.0082 0.0008 0.0001 0.0000 0.1027 0.3946 0.3956 0.1694 0.0382 0.0046 0.0003 0.0000 0.0000 0.0 0.0024 0.0 0.0000 0.0001 0.0008 0.0086 0.0399 0.2106 0.5118 0.4659 0.1977 0.0442 0.0054 0.0004 0.0000 0.0000 0.0001 0.0014 0.0117 0.0565 0.1672 0.2690 0.2150 0.0888 0.0198 0.0024 0.0002 0.0000 0.0000 0.0000 0.0005 0.0040 0.0183 0.0467 0.0654 0.0492 0.0200 0.0045 0.0005 0.0000 0.0000 0.0000 0.0000 0.0001 0.0005 0.0024 0.0060 0.0081 0.0060 0.0024 0.0005 0.0001 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0002 0.0004 0.0005 0.0004 0.0002 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000

NDROPSF(P(1))

```
ER-26
```

```
1
 SECPSF2D TEST
 DX= 16.500000 DY= 16.500000 XMIN= -99.000000 XMAX= 99.000000 YMIN= -99.000000 YMAX= 99.000000
 DISCH FRACTION= 1.000000 DXSEC= 33.000000 DYSEC= 33.000000 SIG= 14.042548
DROPSE(P(6)
                                                     +x
 0.0
        0.000000.0
                      0.00000.0
                                    0.0000 0.0
                                                  0.0000 0.0
                                                                0.0000 0.0
                                                                               0.0000 0.0
 0.000.0 0.000.0 0000.0 0000.0 0000.0 0000.0 0000.0 0000.0 0000.0 0000.0 0000.0 0000.0 0000.0
0.0
        0.0000 0.0
                      0.0000 0.0
                                    0.0000 0.0
                                                  0.0000 0.0
                                                                0.0000 0.0
                                                                               0.0000 0.0
 0.0000 0.0000 0.0000 0.0000 0.0000 0.0003 0.0004 0.0003 0.0000 0.0000 0.0000 0.0000 0.0000
        0.0000 0.0
                      0.0000 0.0
                                    0.0071 0.0
                                                  0.0074 0.0
                                                                0.0000 0.0
                                                                               0.0000 0.0
 0.0000 0.0000 0.0000 0.0003 0.0071 0.1049 0.2265 0.1402 0.0148 0.0006 0.0000 0.0000 0.0000
        0.0000 0.0
                      0.0005 0.0
                                    0.2339 0.8705 0.4691 0.0587 0.0019 0.0000 0.0000 0.0000
 0.0000 0.0000 0.0000 0.0006 0.0153 0.1876 0.4844 0.2507 0.0316 0.0010 0.0000 0.0000 0.0000
 0.0000 0.0000 0.0000 0.0001 0.0037 0.0307 0.0630 0.0317 0.0040 0.0001 0.0000 0.0000 0.0000
 0.0000 0.0000 0.0000 0.0000 0.0001 0.0010 0.0020 0.0010 0.0001 0.0000 0.0000 0.0000 0.0000
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                                                                                               +y
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NDROPSF(P(I))
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 0.000.0 0.000.0 0.000.0 0.000.0 0.000.0 0.000.0 0.000.0 0.000.0 0.000.0 0.000.0 0.000.0
 0,000.0 0,000.0 0,000.0 0,000.0 0,000.0 0,000.0 0,000.0 0,000.0 0,000.0 0,000.0 0,000.0 0,000.0
 0.0000 0.0000 0.0000 0.0000 0.0001 0.0010 0.0020 0.0010 0.0001 0.0000 0.0000 0.0000 0.0000
 0.0000 0.0000 0.0000 0.0001 0.0040 0.0317 0.0632 0.0317 0.0040 0.0001 0.0000 0.0000 0.0000
 0.0000 0.0000 0.0000 0.0010 0.0317 0.2514 0.5014 0.2514 0.0317 0.0010 0.0000 0.0000 0.0000
0.0000 0.0000 0.0000 0.0020 0.0632 0.5014 1.0000 0.5014 0.0632 0.0020 0.0000 0.0000 0.0000
0.0000 0.0000 0.0000 0.0010 0.0317 0.2514 0.5014 0.2514 0.0317 0.0010 0.0000 0.0000 0.0000
0.0000 0.0000 0.0000 0.0001 0.0040 0.0317 0.0632 0.0317 0.0040 0.0001 0.0000 0.0000 0.0000
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0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
09:09:13
```

Figure 9. Processing Spot for 100% Discharge $\Delta X = \Delta Y = 2.35\sigma$



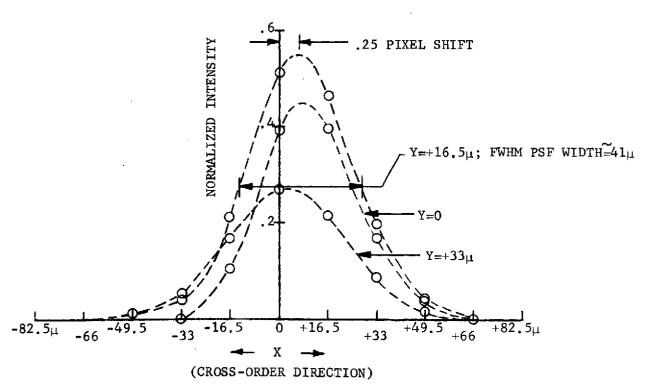


Figure 10. X - and Y - Profiles of Effective PSF 2-17

 $\Delta x = 33 \mu$ and FWHM beam width of 50μ (=2.35 σ), and is the value used for the first two destructive readout simulations performed in this study. From Figure 10 it can be seen that the shift of the peak is about 0.25 pixel in the +x direction and about 0.34 pixel in the +y direction. The y shift (along the order direction) would lead to an error of about 0.019 $\mathring{\rm A}$ in wavelength determination, which would appear to be inconsequential, since it is about 1/5 the wavelength resolution requirement.

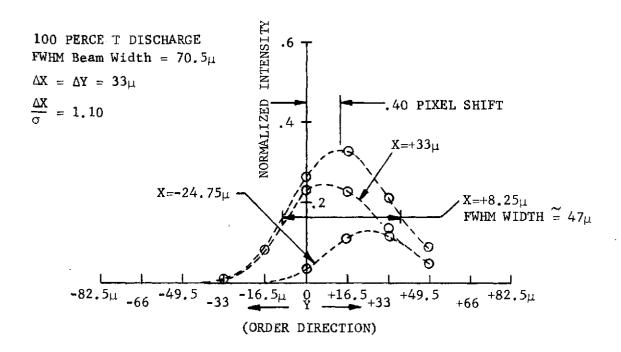
The relative amount of charge readout from a uniformly charged target in a single destructive read compared to a nondestructive read may be calculated from the ratio of the integral Equation (2.7) of the effective PSF for

destructive readout
$$\iint P(\{x-x_i\}, \{y-y_i\}) dxdy$$
 to the integral of the non-destructive readout PSF $\iint_{-\infty}^{\infty} G(x,y) dxdy$.

This ratio can be approximated by the ratio of the sums of the respective PSF array elements in Figures 8 and 9. For 90% and 100% discharge and $\Delta x/\sigma = 1.551$, the ratios are 0.411 and 0.377 respectively.

It was belatedly realized that the ratio $\Lambda x/\sigma=1.551$ is in error, since the FWHM width of 50μ , which was given to us as a "measured beam width", should be interpreted as the effective PSF width in the context of our math model, not the readout beam width. (The measurement consisted of scanning across a very narrow line target, of the order of 5-10 μ in width, which gives the one-dimensional effective PSF.) The above value of $\Delta x/\sigma$ leads to an effective PSF FWHM width of approximately 41μ , about 20 % too narrow, as can be seen from the PSF profiles in Figure 10.

The correct value of beam width was found by computing PSF arrays, varying the beam width parameter. The results show that a FWHM readout beam width of 70.5 μ yields an effective PSF FWHM width of approximately 50 μ . The corresponding PSF profiles are shown in Figure 11. Note that the widths are different in the two directions, being wider in the x-direction, which can be explained by the fewer previous reads in the negative x half-plane than in the negative y half-plane (see Figure 3).



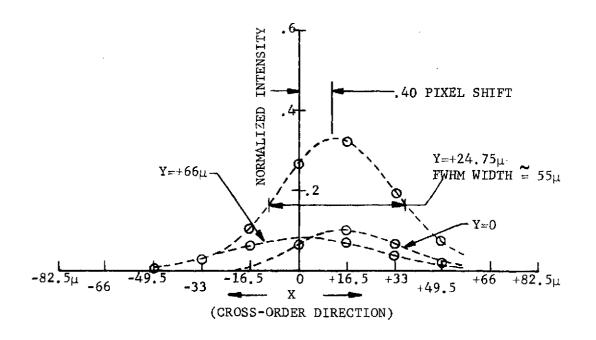


Figure 11. X - And Y - Profiles Of Effective PSF

The peak shift of 0.4 pixel in both directions is somewhat greater and the peak amplitude lower than in the previous case because of the increased discharge overlap. This PSF was used to rerun the destructive readout simulation at $\lambda = 2000 \text{\AA}$.

At the request of NASA, a simulation was also done for an effective readout PSF width of 100μ . (This actually prompted the reexamination of the proper definition of PSF width discussed in the preceding.) The profiles for this width (in the x-direction) are illustrated in Figure 12. The width asymmetry, peak shift and reduction in peak amplitude are even more pronounced. Most of the increased width is in the order direction, which may lead to slightly reduced resolution within an order. This would be most noticeable at λ =1216Å where the UV converter performance is best. The increased spread in the crossorder direction is not enough to significantly increase the order overlap, or, indeed, alter the results of the simulations with the 41μ width. This is borne out by the simulation results (see Section 5.). Again, the shift is mostly in the cross-order direction which does not affect the accuracy of wayelength determination.

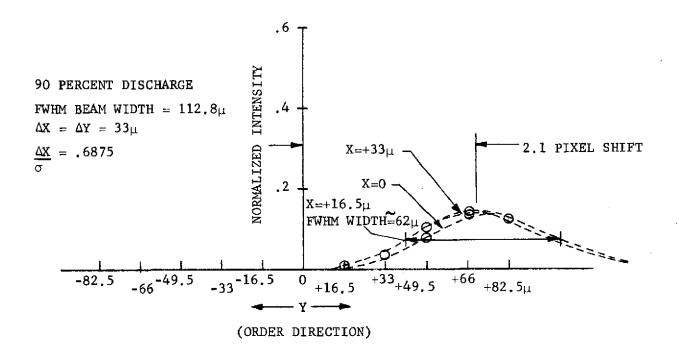
2.3 UV CONVERTER

2.3.1 Introduction

The NASA-furnished converter data was provided in the form of a square wave response (SQR) measurements at four wavelengths: $\lambda = 1216 \text{\AA}$, 1608\AA , 2000\AA and 2500\AA . Sine wave response (SWR), or MTF, which is necessary for the performance calculations, was not directly given but was contained in the "Detector MTF" data of Data Sheet 1 of Reference 2, which consists of the cascaded converter and SEC vidicon MTF's. Since the latter had been computed assuming nondestructive readout of the SEC target, it was necessary to redo the detector MTF calculations.

The calculation of the converter MTF was accomplished in several steps:

- a. Conversion of SQR to SWR via the Coltman formula (Reference 3).
- b. Fitting the resulting SWR curves to an empirical formula



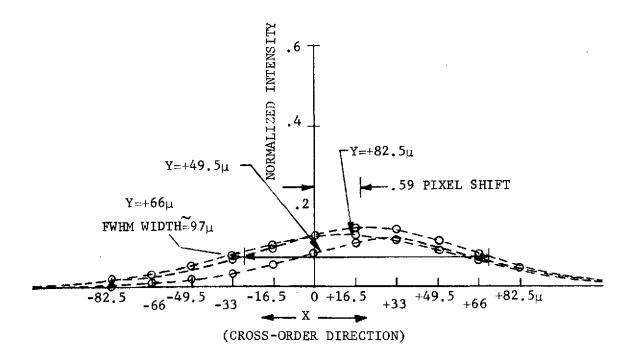


Figure 12. X - And Y - Profiles Of Effective PSF

$$M(s) = \exp \left[-(s/s_c)^n\right]$$
 (2.11)

which has been shown by Johnson (Reference 4) to represent the MTF's of a wide variety of optical and electro-optical imaging devices by suitable choice of the "MTF index" n and "frequency constant" s_c, and

c. Re-inverting the best fitting "Johnson-formula" MTF curves back to SQR as a comparison check with the original SQR data.

2.3.2 MTF Derivation from Square Wave Response Date

The NASA-furnished SQR curves for the UV converter at the four wavelengths of interest are shown in Figure 13. The dotted portions are extrapolations for the purpose of calculating SWR's via the Coltman formula, which is given by

$$M(s) = \frac{\pi}{4} \left[N(s) + N(3s)/3 - N(5s)/5 + N(7s)/7 + N(11s)/11 - N(13s)/13 - N(15s)/15 - N(17s)/17 + N(19s)/19 - \dots \right]$$
(2.12)

where M is the SWR at spatial frequency s, and N is the SQR. At low spatial frequencies, the higher square wave harmonics contribute more than at high frequencies - hence the need for extrapolation of the SQR data. The SWR's thus calculated are shown in Figure 14. (These are the "best fitting" curves to the Johnson formula; the corresponding modulation indices and frequency constants are also noted in the figure.)

2.3.3 Best Fit to Johnson Formula

The calculated SWR curves were plotted on log-log paper as $-l_{\rm nM}(s)$ versus s. Equation (2.11) thus plotted appears as a straight line. The intercept $-l_{\rm nM}=0$ yields the frequency constant $s_{\rm c}$, the 1/e point on the SWR curve, while the slope is proportional to the modulation index n. "Best fitting" (in the sense of matching by eye) straight lines were superimposed on the data and $s_{\rm c}$ and n determined in the above manner.

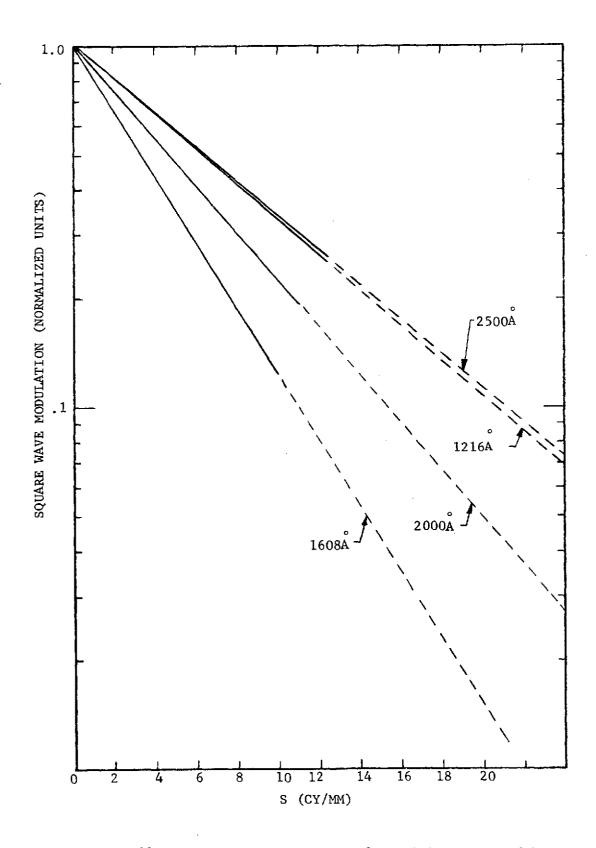


Figure 13. Square Wave Response of Proximity Focussed Converters Average of Bendix Tubes #401, 402, 403-25, 407X

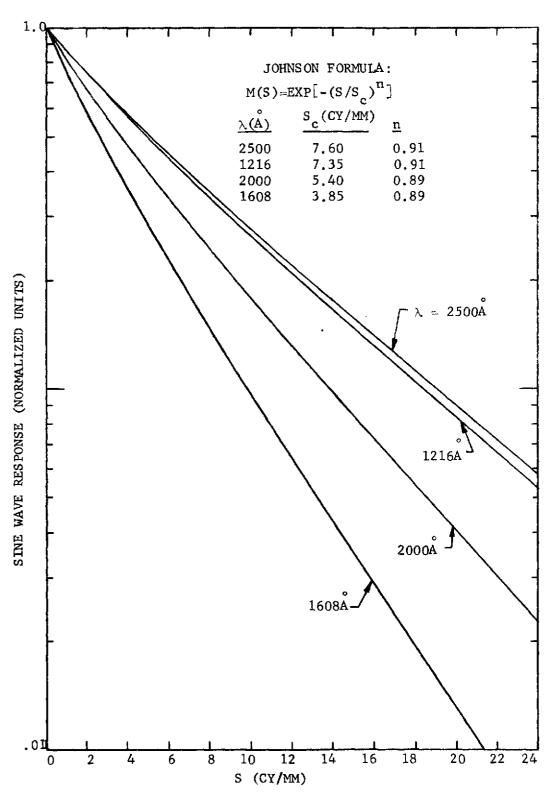


Figure 14. Sine Wave Response of Proximity Focussed UV Converter (Calculated from Square Wave Response Data and Fitted to Johnson Formula)

2.3.4 Re-Inversion to SQR - Comparison with Original Data

The "best fitting" Johnson formula representations of the SWR data shown in Figure 14 were re-inverted to SQR data using the familiar sine wave expansion of a square wave:

$$N(s) = \frac{4}{\pi} \left[M(s) - M(3s)/3 + M(5s)/5 - M(7s)/7 + \ldots \right]$$
 (2.13)

and compared with the original SQR data of Figure 13. Agreement was within 1% over the unextrapolated frequency range.

2.4 GUIDANCE PSF

2.4.1 NASA-Furnished Specification of Truncated Gaussian Servo Jitter PSF

The guidance PSF arising from a stellar point source smeared by servo jitter has been specified by NASA to be circular Gaussian with $\sigma = 0.5~\text{sec}$. This is truncated at the entrance aperture of the spectrograph. The circular aperture of radius $r_0 = 1.5~\text{sec}$. was chosen for study.

At the camera focal plane, the above parameters become $\sigma = 70.7\mu$ and $r_0 = 212.1\mu$.

2.4.2 MTF Derivation

Boggess (Reference 2) calculated the one-dimensional line spread function in the order direction for the truncated Gaussian PSF, which is an error function, and also the corresponding MTF. However, the image at the SEC faceplate is smeared by the two-dimensional PSF; hence, we redid the calculation.

It turned out that our result differed only slightly from those of Boggessless than 1% - in the spatial frequency range 0-14 cy/mm (the system MTF is
dominated by the converter MTF, and drops below 0.01 above 14 cy/mm). Indeed,
both calculations differ from the Gaussian MTF (no truncation) by less than
1% in this frequency range. Above approximately 40 cy/mm, the truncated
Gaussian MTF begins to depart significantly from the Gaussian function,
reaching zero at 51.75 cy/mm, with "side lobes" above this frequency.
(Remember that the MTF is equivalent to the Fraunhofer diffraction pattern
modulus.) Hence, our derivation by Hankel transform is of academic interest

only. The work done is briefly summarized below. Additional material is given in Appendix A.

Since the guidance PSF is radially symmetric, the MTF may be calculated by the finite Hankel transform

$$M_g(s) = \frac{1}{\sigma^2} \int_0^{r_0} J_o(2\pi r_o s) r \exp(-r^2/2\sigma^2)$$
 (2.14)

where \mathbf{J}_{o} is the Bessel function of the first kind and zero order.

This integral was evaluated by partial integration (Appendix A) obtaining the asymptotic expansion

$$M_g(s) \approx \exp(-2\pi^2\sigma^2s^2) - \exp(-r_o^2/2\sigma^2)\sum_{n=0}^{\infty} (-4\pi^2\sigma^2s^2)^n \frac{J_n(2\pi r_o s)}{(2\pi r_o s)n},$$
 (2.15a)

which gives explicitly the expected Gaussian MTF in the limit $r_0/c\gg 1$. An alternative derivation found in the literature (Reference 4) gives the result

$$M_{g}(s) \approx \frac{(r_{o}/\sigma)^{2}}{\exp(r_{o}^{2}/2\sigma^{2})} \sum_{-1 \text{ n=o}}^{\infty} (r_{o}/\sigma)^{2n} \frac{J_{n+1}(2\pi r_{o}s)}{(2\pi r_{o}s)^{n+1}}, \qquad (2.15b)$$

which yields the Fraunhofer diffraction pattern of a clear circular aperture in the limit $r_0/\sigma \ll 1$. The latter asymptotic expansion is obtained also by partial integration but with the u and dv factors interchanged with respect to those chosen in this author's derivation (see Appendix B).

Both expressions were programmed for numerical evaluation. However, due to limitations in the accuracy of the IBM SSP subroutine employed to calculate the $J_{\rm n}$ in the small argument region, this effort was abandoned, and direct numerical integration of Equation (2.14) using Simpson's rule was programmed. The resulting radial MTF for guidance smear is illustrated in Figure 15.

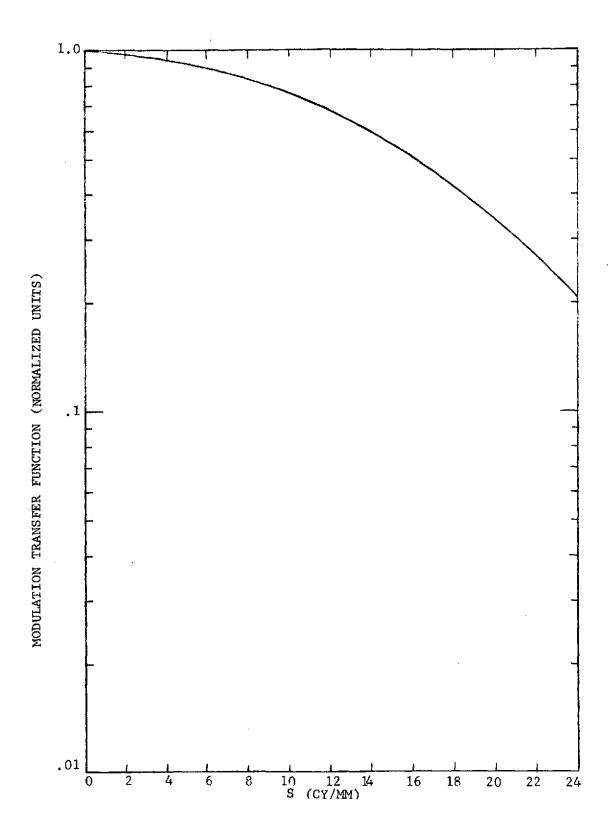


Figure 15. Point Source Guidance MTF

2.5 UV SPECTROGRAPH

The UV spectrograph consists of crossed echelle and concave spherical gratings. In this study, the spectrograph optical performance degradations were assumed to be negligible. NASA-generated spot diagrams indicate that geometrical aberrations in the spectrograph result in image smear that is small compared to smear from the other system components, in particular, the guidance and UV converter smear. Our experience at Perkin-Elmer with the design and fabrication of instruments employing similar grating spectrographs. suggests that the off-axis geometrical aberrations may be more serious than indicated by the NASA spot diagrams. However, Perkin-Elmer has not investigated the particular case of the IUE spectrograph design, since it is beyond the scope of this study.

"Blaze angle falloff" or "ripple", the single slit intensity (sinc²) function, was also to be included in the math model. However, the NASA-furnished unsmeared echellogram data includes this in the order direction already, making it unnecessary to add to the Perkin-Elmer model. However, the NASA data does not include the ripple factor for the cross-order direction. The sinc function squared reaches its half-maximum value at $\pi sp/\lambda \cong 0.463\pi$, where s here is the slit width, and p = $\sin\theta$ -sin θ with θ and θ being the angle of incidence and diffraction angle respectively. Thus, at the half-maximum point $\rho_{1/2} \approx 0.463\lambda/s$. For the spherical grating $\lambda/s \approx \lambda/d$, where 1/d is the grating frequency $(3.3802x10^3 \text{cm}^{-1})$ for the short wavelength grating and $2.3314x10^3 \text{cm}^{-1}$ for the long wavelength grating). At the short and long wavelengths of $\lambda = 1400\text{Å}$, and 2500Å, $\rho_{1/2} \approx 0.0219$ radians and 0.0271 radians, which correspond to half-maximum widths at the camera focal plane of 14.9mm and 18.4mm.

Hence, the falloff in the cross-order direction is not negligible, and should be included in a calibration subsystem for the operating IUE hardware (or software). We have not included it in the Perkin-Elmer simulation model since it is not of central concern in this study.

2.6 SYSTEM MTF AND PSF

The component MTF's discussed in the preceding paragraphs, with the exception of the destructive readout MTF (actually the complex optical

transfer function, or OTF, since the PSF is asymmetric in this case), were cascaded together for input to the simulation program. They are illustrated in Figure 16 for the four converter wavelengths.

The destructive readout OTF (or PSF, depending on the method of simulation) was used as input in an intermediate simulation in a two-step process consisting of the smear due to the readout process alone, followed by the additional smear of the cascaded converter and guidance components. This is discussed more fully in the following subsection (Paragraph 2.7).

The system PSF (again minus the SEC readout) was obtained by Hankel transforming the cascaded converter and guidance MTF's. These are shown in Figure 17 for the four converter wavelengths. These were calculated for the purpose of simulation by the direct convolution method but were not used, since the frequency domain method was alternatively used, as discussed in Paragraph 2.7.

2.7 COMPUTER IMPLEMENTATION

The simulations can be carried out by either direct convolution in the spatial domain or by linear filtering via Fast Fourier Transform (FFT) in the spatial frequency domain, followed by inverse FFT. (The latter process is also referred to as "FFT convolution.") Spatial domain simulation was the method initially chosen. However, the cost per simulation proved to be greater than anticipated to the point of being prohibitive (≤\$250 per simulation). Overlooked in the original decision was the need to interpolate the data and also the processing spot to be convolved which approximately doubled the array dimensions of each. The input echellogram data points had been generated on the SEC readout sampling lattice. At all previously read sample points, the processing array amplitudes were zero, for 100% discharge. SEC readout effective PSF (see Equation (2.7)) is non-zero between the sampling points, but this information is lost in the digital approximation to the continuous convolution integral, unless one samples the PSF between the zeroes. This means, since the echellogram and PSF must be defined on the same sampling lattice, that the echellogram must be interpolated to whatever density

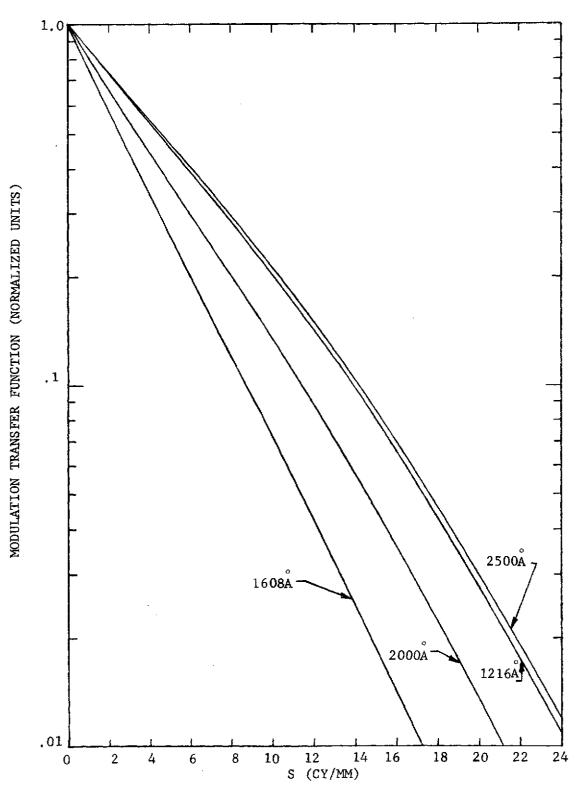


Figure 16. Cascaded Point Source Guidance And UV Converter MTF's

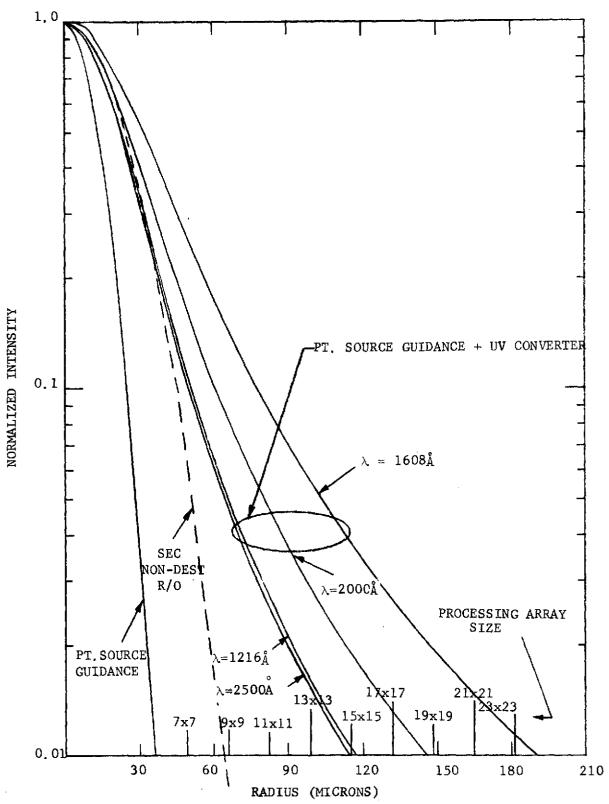


Figure 17. Instrument PSF's (not including destructive R/O)

desired for the sampling of the PSF. Thus, for example, at λ = 1216Å the processing array size, requirement (truncating the PSF array at \approx 2% of the peak value) went from 7x7 to 13x13 (see Figure 17). At λ = 2000Å, the required size for comparable accuracy becomes 17x17.

Essentially, the digital computation process introduces a sampling in addition to that of the readout. (Again, for convenience, we discuss the one-dimensional case. Generalization to two dimensions is straightforward as in Section 2.2.3.) The convolution integral Equation (2.6) is replaced by a sum, i.e., at the k'th beam address

$$\int_{-\infty}^{\infty} Q(x) P_{k} (\{x-x_{i}\}) dx \cong \Delta x \sum_{m=0}^{M-1} Q(x_{m}) P_{k} (\{x_{m}-x_{i}\})$$

where the x_{m} are the M points on the computational lattice (M = 2N-1, where N is the dimension of the readout lattice).

The two-dimensional form of this discrete convolution was performed using program "CONVOL" from Perkin-Elmer's Digital Image Processing Programs (DIPP) library for the spatial domain computations giving the result of the destructive readout process alone, without the other contributions to smear. The latter, namely the guidance and converter smear, were simulated by FFT convolution of these with the echellogram smeared by destructive readout.

In the frequency domain, the Fourier transform of the above integral is given by the product of the Fourier transforms of Q(x) and P(x), i.e., Q(s) and P(s). The discrete transforms are equal to the values of Q(s) and P(s) at the points s_m ($m=0, 1, \ldots, M-1$) on the frequency sampling lattice of spacing Δs which is related to the spatial sampling lattice by $\Delta s = 1/M\Delta x$.

The discrete Fourier transform of $Q(x_i)$, denoted as $\hat{Q}(s_i)$, is

$$\hat{Q}(s_i) = \Delta s \sum_{m=0}^{M-1} Q(x_m) \left[exp(-\frac{2\pi s_i}{M}) \right]^m$$

and similarly for $\hat{P}(s_i)$.

In this study, the system PSF was constructed by cascading the component MTF's (Fourier transforms of the PSF's) and then inverse transforming this result to obtain the PSF. Hence, the switch to frequency domain processing required only the calculation of the echellogram transform.

Another program package in the DIPP library called "XFORM" was used for the frequency domain processing. It consists of a set of subroutines which reads the input "scene" (echellogram in our case), performs the two-dimensional discrete Fourier transform via FFT, multiplies this by the processing OTF (system OTF), which is complex in this case because of the asymmetrical destructive readout PSF, performs the inverse transform of the result and outputs to LSIG magnetic tape. Optionally, the echellogram transform may be saved on tape or disk in case it is desired to process the same scene with more than one OTF, which was the case here. To satisfy the discrete Fourier transform requirement of periodicity and continuity of the scene at the edges (the points \mathbf{x}_0 and \mathbf{x}_{M-1}), a raised cosine rolloff to zero intensity was applied to the echellogram borders extending nine samples in from each edge.

The echellograms 256 x 400 were processed in 256 x 256 "chunks," overlapping by 112 records (order direction) in the center. The spatial frequency sampling interval and maximum spatial frequency for an N x N image are given by $\Delta F = 1/N*\Delta X$ and $F_{max} = (N/2)*\Delta F$, where ΔX is the spatial sampling interval. In the case of N = 256, $\Delta X = 16.5\mu$, $\Delta F = 0.23674$ cy/mm, and $F_{max} = 30.30303$ cy/mm.

SECTION 3

PREPARATION OF INPUT ECHELLOGRAM

The NASA furnished tape used in the subsequent simulations contains three files: the first two consisting of slit scan spectra, "crowded" and "uncrowded" absorption spectra in the UV, and the third a simulated "unsmeared" echellogram made from the former slit scan spectrum by geometrically transforming the various orders into the echelle format, but without smear due to IUE system degradations.

The echellogram tape was in VICAR format, i.e., each data point was written as one byte. Some problems were encountered in the process of writing a program to read this unfamiliar format. These were eventually solved and a section of the tape was rewritten in LSIG-compatible format (two 6-bit bytes, reversed) and the amplitudes were multiplied by a factor of 32 to provide sufficient grey level amplitude for the LSIG. A 150 x 200 section from the bottom of the format was taken where the orders are most closely spaced. This is illustrated in Figure 18 which is an LSIG reproduction of the NASA echellogram.

The echellogram subsection was next linearly interpolated two-to-one in both dimensions to obtain sufficient sample density for the digital convolution purposes as discussed in Section 2.6, yielding an array almost four times as large, 299 points x 397 records. (One would expect dimensions of (2M-1) x (2N-1) in an array generated by linear interpolation from an MxN array -- in this case, 299 x 399.) However, the interpolation program terminated after 397 records due to a system bug.)

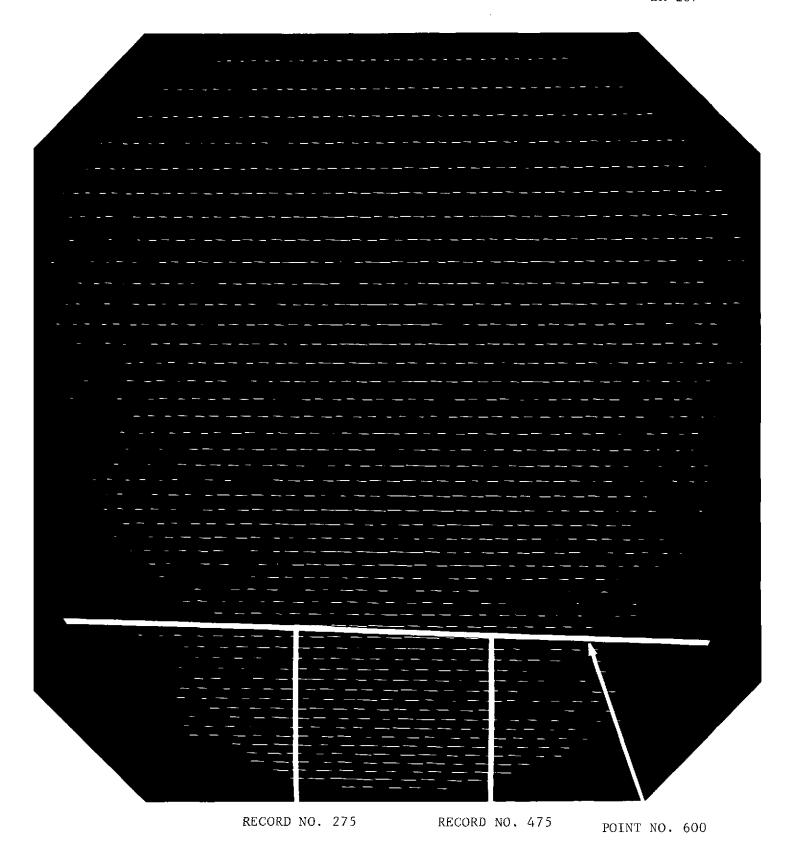


Figure 18. NASA Echellogram "REDPSF" (750 x 750) Reproduced on LSIG, Showing Subsection Used for Simulations

the relevant parameters of wavelength, spatial sampling intervals for the SEC readout and for computation, PSF and R/O beam widths, spatial frequency sampling interval, etc.

Negative transparencies of all simulations were made on the LSIG using a clear square writing mask.

The simulation outputs are shown in the deliverable photographs and positive transparencies which accompany the report in a separate package. Tape dumps of selected subsections of the simulated echellograms are given in Figures A-1 to A-7 of Appendix A.

SECTION 5

DISCUSSION OF RESULTS

5.1 EFFECTS OF DESTRUCTIVE READOUT

The major results to be noted here are, first, that the wavelength error introduced by the pixel shift due to PSF asymmetry is small for the case of the 50 micron width. As discussed in Paragraph 2.2.5, the shift of the peak of the effective PSF is less than 1/2 pixel in both the order and crossorder directions. However, this does not give the whole story. In Figure 19 a portion of a single order, smeared by the SEC readout alone (Simulation 2) and integrated across the width of the order (simulating a slit scan) taken near the bottom of the echelle format, was plotted in the order direction. For comparison, the corresponding portion of the unsmeared input (Simulation 1) was also plotted. The abscissa units are pixel numbers for the interpolated echellogram (remember that 2 interpolated pixels = 1 readout pixel) and the ordinate is grey level (x32 relative to the NASA-furnished data). It is evident from this comparison plot that the spectra are nearly identical. The SEC readout spectrum is shifted by approximately one readout pixel with respect to the input, whereas the shift of the PSF peak was less than 1/2 pixels as noted above. In addition, there is some smoothing of the data. The peaks and valleys agree in amplitude to better than one percent. Indeed, it appears that if the shift were taken out, the two spectra would agree within one percent throughout. We remind the reader that the normalized OTF for SEC readout was used for the simulations, and that a gain reduction factor of 0.411 (see Paragraph 2.2.5) should be applied to the curve for SEC readout. However, this is not a loss of modulation, but merely gain.

Hence, the only significant result of the destructive readout process for spectroradiometric data analysis as predicted by our linear model (assuming sufficient noise-free gain elsewhere in the system chain) is the shift of one

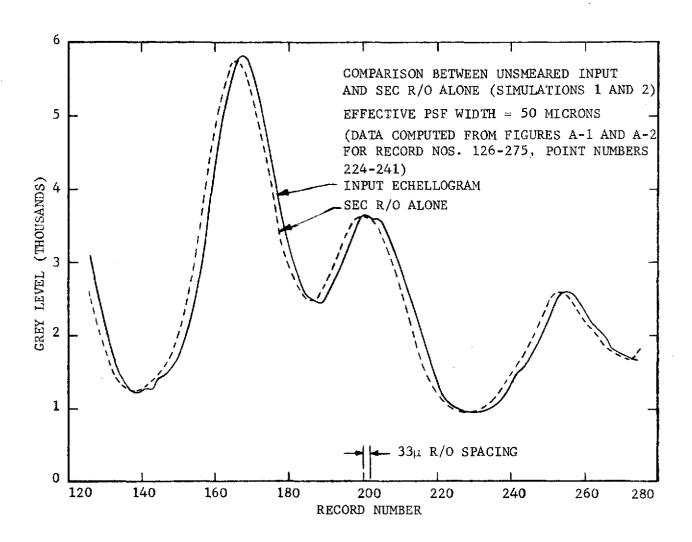


Figure 19. Simulated Slit Scan of Echelle Order Along Order Direction

readout pixel. The smear resulting from the SEC readout does not appreciably affect the resolution along the order direction, if the energy spread in the cross-order direction is integrated by slit scanning. For the case of the 100 microns PSF width, the smear has increased enough in the cross-order direction to cause a small degree of order overlap in simulation of the SEC readout alone (see the printout in Figure A-3). Because of this, and because of insufficient time remaining in the contract, the slit scan calculation done to obtain Figure 19 was not repeated. However, in this case, one would expect a result similar to the 50 microns case, since the overlap is not serious. Some loss in modulation should be expected since the PSF width in the order direction is doubled.

5.2 EFFECTS OF GUIDANCE AND UV CONVERTER SMEAR

These components, when convolved with the echellogram data smeared by the SEC vidicon, give rise to the greater part of the total smear, with resulting order overlap, which can be seen in both the photographs and the computer printouts of Appendix A. We have also plotted representative profiles in the cross-order direction near the bottom center of the format. These are shown in Figure 20.

The wavelength dependence can be observed by comparing simulations 8 and 9 (reference Table 4-1). As one would expect, the greatest smear occurs for the $\lambda = 2000 \text{Å}$ case, where the converter performance is worst.

The result of doubling the SEC readout PSF width from 50 to 100 microns is largely masked by the converter and guidance smear contributions, as can be seen by comparing Simulations 4 and 5.

A peak shift of approximately one readout pixel in the cross-order direction can also be observed in Figure 20.

Order overlap in the complete system simulations is significant enough that one would expect a slit scan calculation similar to that done for the SEC readout alone (Figure 19) to be in error, particularly for a case integrating



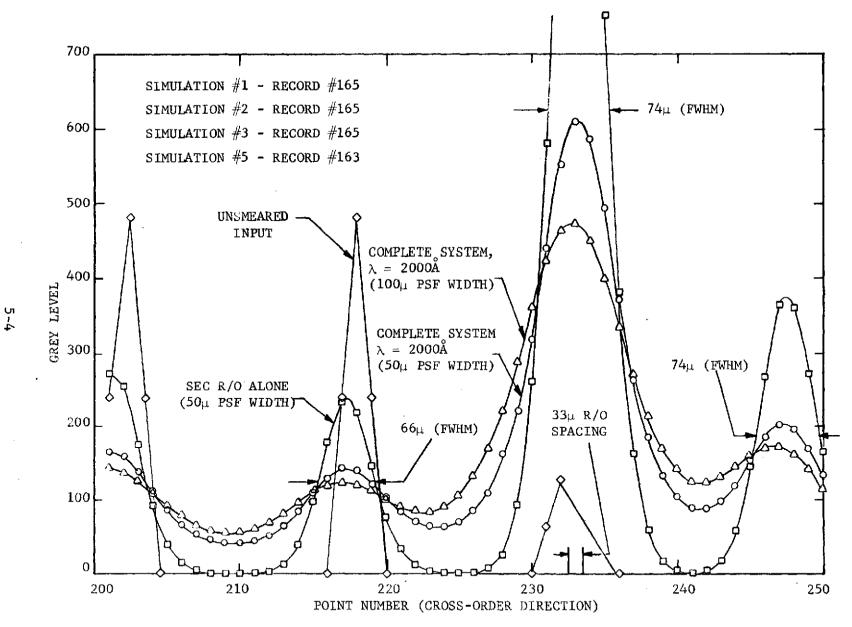


Figure 20. Simulation Profiles in Cross-Order Direction at Bottom Center of Echelle Format

a weak profile adjacent to a strong one. A suggested approach would be to try enhancement filtering in the cross-order direction, wherever the overlap is serious.

SECTION 6

SUMMARY AND CONCLUSIONS

This study program has resulted in the generation of a linear mathematical model for computer simulation of the optical performance of the IUE Scientific-Instrument imaging chain. A series of computer programs has been written to implement the model, and a number of simulated echellograms were generated demonstrating the major effects of performance degradations due to the several imaging components. In particular, an algorithm was developed to represent the two-dimensional destructive readout process in the SEC vidicon camera by an effective PSF which, to a good approximation, is space-invariant.

The major conclusions of this program are:

- a. Wavelength determination error due to the pixel shift arising from destructive readout is predicted to be approximately one readout pixel (33 micron width), or approximately 0.06Å in wavelength, for the case where the effective PSF FWHM width is taken to be 50 microns.
- b. Order overlap is principally due to the smear of the guidance and converter components, and may be a significant problem at the bottom of the echelle format, particularly for the case of a weak order profile adjacent to a strong one. Enhancement filtering in the cross-order direction may provide help in this instance.
- c. Radiometric error due to the discharge overlap of the destructive readout is predicted to be negligible, provided that the assumption of a linear readout process is a good approximation to reality, and also that there is sufficient noise-free gain in the system chain to overcome the loss in gain due to destructive readout. Radiometric error may result from aberrations in the spectrograph (which were ignored in this study) and also in the electron beam focus of the SEC vidicon.

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APPENDIX A

COMPUTER PRINTOUTS OF SIMULATIONS 1-7

Figures A-1 through A-7 are dumps of selected portions of the echellogram simulation tapes for simulations 1 through 7 (of Table 4-1) near the bottom center of the echelle format.

The point and record numbers are those of the computational lattice which has dimensions of 256 points x 400 records. The lattice spacing in both directions is 16.5 microns. The point numbers increase horizontally (crossorder direction) from left to right, while the record numbers increase vertically (order direction) from top to bottom.

The simulated slit scan discussed in Paragraph 5.1 and shown in Figure 19 was hand calculated from swaths of data in Figures A-1 and A-2 between point numbers 224-241, records 126-275.

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TAPE 812 - NASA INTERPOLATED ECHELLOGRAM REOPSF, 32X (SIMULATION INPUT)

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Figure A-1. Echellogram Subsection - Tape No. 812

SECTION 4

SIMULATIONS

The interpolated echellogram made in Task II was first convolved with the effective PSF for destructive readout yielding an intermediate echellogram on LSIG magnetic tape. At this point, it was decided to switch to FFT convolution processing to save money on computer time, which, as we have noted in Section 2, was prohibitively expensive for direct convolution because of the large size of the PSF processing array required.

Destructive readout simulations at converter wavelengths of $\lambda=1216 \mbox{\AA}$ and 2000Å were completed via FFT convolution using the cascaded MTF's for the converter, and guidance components as inputs.

This was followed by a nondestructive readout simulation at $\lambda=2000 \text{\AA}$ which was done entirely by FFT convolution.

At a meeting with NASA, the above results were presented, and plans for modifying and limiting the schedule of further simulations were made. It was requested by NASA that we do a destructive readout simulation using an effective PSF width of 100 microns (double the width used previously) because the order overlap appeared from the photographs to be less than expected. In the course of selecting the appropriate beam width parameter, it was realized that the effective PSF width and the readout beam width are not the same, as already discussed in Paragraph 2.2.5. After determining the correct beam width parameter for the 100 microns PSF width, it was decided to redo the 50 micron case. This was accomplished by FFT convolution which required the calculation the complex OTF for the SEC readout, due to the asymmetry of the PSF.

A table of simulation data appears in Table 4-1, including the intermediate simulations of SEC readout alone and giving titles, figure numbers, and

TABLE 4-1
SIMULATION DATA

Simulation No.	Tape No.	Fig. No. (Computer Printout)	Title	Sim Type	Eff. Sec. PSF Width (μ)	R/O Beam Width (µ)	Type of Convol- ution	Conv. Wavel. (Å)	Sec R/O Spacing (µ)	Comput. Lattice Spacing (µ)	Spatial Freq. Sampling Interval (cy/mm)
1	812	A-1	Interpolated NASA Echellogram, "REDPSF," 32X (Simulation Input)	•	-	-	-	_	33	16.5	<u>-</u>
2	518	A-2	Destructive R/O Simulation (SEC Alone)	DRO	50	70.5	PFT	-	33	16,5	0,23674
3	255	A-3	Destructive R/O Simulation (SEC Alone)	DRO	100	112.8	FFT	-	33	16.5	0, 23674
4	422	A-4	Destructive R/O Simulation (Complete System)	DRO	50	70.5	FFT	2000	33	16.5	0,23674
5	275	A-5	Destructive R/O Simulation (Complete System)	DRO	100	112.8	FFT	2000	33	16.5	0.23674
6	813	A-6	Non-Destructive R/O Simulation (Complete System)	NDRO	50	50	FFT	2000	33	16.5	0, 23674
7	170	*	Destructive R/O Simulation (SEC Alone)	DRO	41	50	Direct	-	33	16,5	0, 23674
8	888	-	Destructive R/O Simulation (Complete System)	DRO	41	50	Direct + FFT	2000	33	16,5	0, 23674
9	1107	A-7	Destructive R/O Simulation (Complete System)	DRO	41	50	Direct + FFT	1216	33	16,5	0,23674

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ECHELLOGRAM SUBSECTION

TAPE 812 - NASA INTERPULATED ECHELLOGRAM REDPSF, 32X (SIMULATION INPUT)

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Figure A-1 (Sheet 4 of 6)

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D ō ŏ 528 1024 560 1072 592 1120 ō 32 616 1168 ō 640 1216 ō ō ō 648 1232 ō O ō 656 1248 Ó Ö Ô ō 648 1232 536 1072 Ò 640 1216 ā ö ŏ n ō ō 576 1152 624 1168 ò o ŏ ō 616 1232 ō 608 1120 Ö C 656 1312 584 1072 ō ō 688 1376 ē. õ 560 1024 ō 720 1440 544 976 ō ō 4AR Ô ā ō 744 1488 ò ō Õ ō ō ō 768 1536 Ó 776 1552 o 784 1568 O 784 1568 Õ ē ō ō ō 784 1568 Ð ō 760 1520 C c Œ ō 736 1472 Ō Û C a Ò 704 1408 õ 672 1344 ŋ ġ o Õ ŏ 632 1264 Ö ŋ Ó ā ō ō O 592 1184 1 92 ò Ō ō ō 552 1104 0 512 1024 528 ō

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Figure A-1 (Sheet 6 of 6)

ECHELLOGRAM SUBSECTION

TAPE 518 - DESTRUCTIVE RAD SIMULATION (SEC ALGNE), SEC PSF FWHM WIDTH = 50 MICR ONS

	TS: ECS:	201 126		25 75				ELS = 087E	10240 03	0 SU	M = 0	.111	3E 08			•								
783	750	530	295	138	55	18	5	1	0	1	7	31	102	251	458	610	587	417	233	110	44	14	4	ı
806	768	538	297	138	54	18	5	ī	Ō	1	8	33	109	268	489	650	623	440	245	114	45	15	4	1
814	772	537	293	135	53	17	5	1	0	1	8	35	115	283	517	686	655	460	254	118	47	15	4	ì
808	763	527	205	130	51	16	5	1	0	2	9	37	120	296	5 3 9	714	679	475	260	121	47 47	16 15	4	1
789	742	510	274	125	49	16	4	1	0	2	9	3 B	123	303 305	552 555	730 732	692 692	481 478	262 258	121 118	46	15	4	1
759	713	488	261	118	46	15	4	1	0	2	9	38 37	123	301	548	721	679	466	249	113	43	14	4	ī
721	676	450 430	245 228	110 102	42 39	14 13	3	ì	ŏ	2	8	36	119	293	532	700	656		238	107	41	13	4	1
678 634	634 591	400	211	95	36	12	3	ì	ō	ī	8	35	115	282	511	671	628	427	226	102	39	13	3	1
588	547	369	194	86	33	10	3	ī	ŏ	ì	8	33	109	268	480	637	595	403	213	96	37	12	3	1
539	501	336	175	77	29	9	2	1	Ó	1	7	31	102	251	455	596	556	376	198	89	34	11	3	1
489	452	302	156	68	26	8	2	0	0	ì	7	29	94	231	419	549	511	344	181	81	31	10	3	1
438	404	269	139	61	23	7	2	0	0	1	6	26	86	210	181	498	463	311	162	72	27	9	2	ì
390	360	239	123	54	21	7	2	e	0	1	6	24	77	190	344	449	416 374	278 250	145	64 57	24 22	8 7	2	0
344	318	211	109	4 B	18	6	2	0	Ω Ο	1 1	5 4	21 19	70 63	171 154	309 280	404 365	339	227	119	53	20	6	2	ŏ
302	279	185	95	41	15 13	5	1 1	0	ó	i	4	18	57	141	256	335	311	210	110	49	19	6	2	ō
264 231	243 212	160 139	81 70	35 29	10	4 3	ì	Č	ŏ	ì	4	16	53	131	237	310	288	194	101	44	17	5	1	0
207	189	124	52	26	9	3	i	ö	ŏ	1	4	15	49	121	220	287	266	178	91	39	14	4	1	C
189	173	113	56	24	В	2	ī	o	ō	1	3	14	46	113	204	266	245	162	82	35	12	4	1	0
175	160	104	52	22	8	2	1	0	0	1	3	13	43		191	248	228	150	75	32	11	3	1	0
163	149	98	49	20	7	2	Q	O	0	1	3	12	41	100	180	234	215	141	71	30	11	3	1	0
	141	93	46	20	7	Z	0	0	0	c	3	12	39	95	172	224	206	136	68	29 28	10 10	3	1	0
147	136	90	45	19	7	2	0	0	0	0	3 3	11	37 36	92 89	166 160	216 209	199 192	131 126	66 64	27	10	3	i	õ
144	133	88 88	45 45	19 19	7	2 2	0	0	0	0	2	11	35	86	155	201	185	122	61	26	9	3	î	ő
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143	132	86	45	19	7	2	ō	č	Č	ō	S	10	32	80	144	187	172	113	57	24	9	3	1	C
143	132	88	45	19	7	2	Ó	0	0	C	2	10	31	77	139	181	166	110	55	23	8	2	1	0
	132	98	45	19	7.	2	٥	0	0	0	2	9	30	75	135	176	162	107	54	23	8	2	ì	0
144	133	89	45	19	7	2	O	0	0	٥	2	9	30	73	133	173	161	107	- 54	23	8	2	1	0
146	135	90	46	20	7	2	ū	0	O.	0	2	9	30	74	133 136	174 178	162	108 110	55 56	24 24	9	2	l l	Ö
150	1 40	94	48	21	7	2	0	0	0 0	0	2	9 10	31 31	75 77	139	182	165 169	113	58	25	9	3	î	ŏ
156	146 154	98 104	50 53	22 23	8 8	2	1	Ö	0	ŭ	2	10	32	79	143	186	173	115	59	25	ģ	ã	ī	ō
165 176	165	112	58	25	9	3	i	ő	ő	ŭ	2	10	33	81	146	191	178	119	61	26	9	3	1	0
192	181	123	64	28	10	3	ĩ	ō	ō	Ċ	2	10	34	84	152	199	186	125	64	28	10	3	1	0
214	201	137	72	31	11	3	ì	O	C	0	3	11	36	88	160	210	196	131	68	29	11	3	1	٥
241	226	154	81	35	13	4	1	۵	0	c	3	12	38	93	169	221	206	138	71	31	11	3	1	0
272	255	174	91	40	14	4	1	0	0	Ţ	3	12	40	98	178	233	218	146	76	33	12	3 4	1 1	0
308	288	196	102	44	16	5	Ţ	O.	0	1	3	13 15	43 48	105 115	190 207	249 271	233 253	157 170	82 88	35 38	13 14	4	i	G
347	3 2 3	219	115	50	18 20	5	1	0	0	l l	4	18	-	128	227	295	274	185	96	41	15	4	i	ŏ
388 430	361 400	245 271	128	55 61	22	6	ì	Ö	o o	î	6	21		142		321	297	200	103	45	16	5	ī	ō
473	440	297	154	67	24	7	ž	ŏ	ő	î	6	23	88	155	270	347	322	216	112	48	18	5	ī	G
518	480	323	167	72	26	8	2	0	0	2	7	25	73	168	292	375	347	233	121	52	19	5	1	0
562	520	349	180	78	28	8	2	0	0	2	7	27		180	313	403	373	250	129	56	20	6	1	0
602	556	372	191	82	30	9	5	٥	0	2	ė	28	83	191	334	430	397	266	137	59	21	6	1	1 .
637	586	391	200	86	31	9	2	o o	0	Š	8	30	88	202	353	454	419	280	144	62	22	6	2 2	1 1
663	609	405	207	88	32	9	Z	Ó	0	2	9	31 34	93 98	213 223	371 387	476 495	438 454	292 302	149 154	64 66	23 24	7	Ž	Ţ
682	626	415	211 212	90 90	32 33	9	2	0	0 ถ	2	10	36	104	233	401	510	467	309	157	67	24	7	2	ì
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Figure A-2. Echellogram Subsection - Tape No. 518

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0 1 5 18 43 78 103 95 Figure A-2. (Sheet 2 of 6)

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175 164 123

176 161 118

181 161 115

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293 216 127

359 255 144

423 295 161

362 244 128

218 115

278 154

288 159

191 117

181 174

197 165

197 207 168 111

213 219 174 111

272 204

323 315 229 132

349 337 242 137

455 430 297 160

457 430 294 156

444 415 280 147

429 400 270 141

410 382 257 135

302 281 190 100

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ECHELLOGRAM SUBSECTION

TAPE 518 - DESTRUCTIVE R/O SIMULATION (SEC ALCNE). SEC PSF FWHM WIDTH = 50 MICR ONS

	TS: ECS:	226 126		:50 :75				XELS 1087E		1400 5	iUM =	0.111	3E 08											
c	1	7	30	98	241	437	572	631	364	100	0.7		1.0			•			22		• • •		•	250
Ö	l	6	28	95	221	400	523	531 485	356 324	185 168	82 74	31	10	3	1	0	1	6	22	62	138	234	290	259
Ö	i	6	25	83	203	367	480	445	297	154	68	28 26	9 8	2	1 C	O C	2 2	7 7	24 26	68 74	151 165	256 280	317 347	283
ŏ	î	5	23	76	187	338	442	409	274	142	62	24	7	2	ŏ	ŏ	2	á	28	81	180	305	378	310 337
e	i	5	21	70	172	312	407	377	252	131	57	22	7	2	ŏ	ň	ž	9	31	88	196	331	409	363
ō.	ı	5	21	65	158	287	375	347	232	120	52	19	6	ĩ	ō	ā	2	1ó	34	96	211	354	435	385
0	1	4	19	60	147	265	347	321	213	109	47	17	5	ī	Õ	ì	3	11	37	102	223	371	455	401
Ö	ì	4	17	56	137	248	324	298	197	100	42	15	4	1	0	ì	3	11	38	106	230	383	468	412
0	1	4	16	53	132	235	305	2B1	185	93	39	14	4	1	9	Ł	3	11	39	107	233	388	475	416
0	1	4	15	51	124	224	292	269	177	89	38	14	4	1	0	1	3	11	39	107	234	389	475	416
0	i	3	15	49	120	217	283	261	172	87	37	13	4	1	0	I	3	ιi	38	107	233	387	472	413
0	ı	3	15	48	118	213	279	258	171	87	37	13	4	1	0	L	3	11 -		106	230	382	466	407
Č	1	3	15	48	118	213	279	259	172	88	37	14	4	1	0	1	3	11	38	104	226	375	458	399
0	l l	3	15	49	119	216	282	262	174	89	38	14	4	1	0	l	3	11	37	102	222	368	448	391
0	1	4	15 15	49 50	121	219 223	286 291	265 270	177 180	90	38 39	14	4	1	ç	1	3	11	37	101	216	360	438	381
Ö	1	4	16	51	126	228	299	278	186	92 95	41	14 15	4	1	0	1	3	11	37	100	215	353	428	373
ñ	i	4	16	53	130	236	310	288	193	99	42	15	4	1	0	1	3	11 12	38 39	101	214 213	348 343	420 409	364
ñ	ī	4	17	55	135	245	320	297	199	102	44	16	5	i	Ö	i	3	13	41	105	212	335	396	353 339
O.	ī	4	17	57	139	253	330	307	205	105	45	16	5	í	Ô	ì	4	14	42	105	208	324	378	322
3	ī	4	18	59	145	262	343	319	214	110	47	17	5	ì	Ď	î	4	14	43	104	202	309	358	303
0	ì	5	20	63	153	276	361	335	225	116	50	18	Š	ī	ŏ	ī	4	14	42	101	195	294	338	284
0	1	6	22	69	165	294	383	356	239	123	53	19	6	ĭ	ō	ī	4	15	43	100	188	279	316	264
Ü	ì	7	25	77	179	317	410	380	256	132	57	21	6	1	0	1	4	15	44	100	183	265	296	244
Ü	2	8	28	84	195	343	442	410	276	143	62	22	7	2	0	1	5	16	45	101	179	253	277	226
9	2	9	31	93	213	373	480	445	300	155	67	24	7	2	0	į.	5	17	47	102	177	243	260	210
j	2	10	35	102	234	4 C 8	524	486	327	170	73	27	8	2	i	1	5	18	49	104	175	234	246	196
0	2	11 12	39 44	114 126	259	448	575	533	359	187	81	29	9	2	l	1	6	19	51	106	174	227	233	183
l ł	3	14	48	139	285 315	493 544	632 698	586 647	396 437	206 227	89 98	32	9	2	ļ	į.	6	20	53	109	175	222	222	171
î	3	15	53	153	347	600	768	711	479	249	107	36 39	10 11	2	1	2	6 7	21 23	56	113	177	217	212	161
ī	4	17	59	169	381	657	841	777	523	271	117	42	12	3	1	2	8	26	60 65	119 127	181	216 220	205 201	151
ī	4	18	64	184	414	714	912	843	566	292	126	46	13	3	i	2	9	28	72	139	203	228	202	145 143
1	4	19	69	198	445		982	905	607	313	134	49	14	3	i	2	10	32	80	153	219	241	208	143
1	5	21	74	211	476	820	1047	964	644	331	142	51	15	3	ī	3	11	35	89	168	238	256	215	145
1	5	22	79	224	504	868	1106	1016	678	348	149	54	16	4	1	3	12	39	98	184	258	273	224	148
1	5	23	83	236	529		1158		708	362	155	56	16	4	1	3	13	44	108	203	281	292	234	151
1	6	24	86	246	551		1202		732	373	159	58	17	4	1	4	15	48	120	223	307	314	246	155
1	6	26	90	254	568		1236		748	380	162	58	17	4	L	4	16	54	133	246	335	338	260	160
1	6 6	26 27	92 94	261 264	580 585		1255		755	382	162	59	17	4	1	4	18	59	146	269	364	362	273	165
1	7	28	95	265	584		1259		754 744	380 374	161 158	58 57	17	4	1	5	20	65	159	292	392	385	285	169
i	7	28	95	264	578		1228		726	364	153	55	16 16	4	2	5 5	21	69	171	313	418	407	297	172
ī	7	29	96	262	569		1194		701	350	147	53	15	4	2 2	6	23 24	74 79	183 194	333 353	443 468	42B	308	176
ī	7	29	96	259	556		1149		670		140	50	14	3	2	6	26	84	205	373	498	448 4 69	319 330	179 183
2	7	30	97	255	539		1096	98C	534	314	131	47	14	3	2	6	27	88	216	392	516	488	340	187
2	8	30	96	250	520		1036	922	594	293	122	44	13	3	Ž	7	28	92	225	409	537	505	350	190
2	В	31	97	245	500	B03	975	863	554	273	114	41	12	3	Ž	7	29	95	233	422	553	519	356	192
2	8	32	97	241	482	161	914	804	514	253	105	37	11	3	2	7	30	97	238	430	562	524	358	191
2	9	33	99	239	465	720	854	745	475	232	96	34	10	2	2	7	30	98	238	430	561	521	352	186
2	9	34	100	235	448	678	793	686	434	212	87	31	9	2	2	7	30	96	235	423	550	509	342	179
2	10	35	101	232	430	637	733	629	396	192	79	28	8	2	2	7	29	93	227	408	530	489	327	170

Figure A-2 (Sheet 4 of 6)

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79	142	182	164	106	52
73	130	167	151	97	48
67	120	154	139	90	44
62	111	142	129	83	41
58	103	133	120	78	39
54	97	125	113	73	36
51	92	119	108	70	35
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48	86	112	102	67	34
48	87	113	103	68	35
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67	121	158	145	96	49
71	128	167	154	102	53
76	137	179	165	111	57
83	150	195	181	122	63
93	167	217	201	136	70
05	187	243	224	150	76
19	210	269	248	166	85
34	233	297	273	182	94
49	257	327	300	200	103
53	283	360	330	220	114
78	309	394	361	241	124
93	336	428	393	261	134
09	363	463	424	282	145
25	391	499	457	303	155
43	421	535	489	324	165
61	450	570	519	343	175
77	476	601	547	361	184
91	498	630	572	377	192
03	520	657	596	393	199
15	540	681	618	406	206
26	557	701	634	415	210
35	569	713	643	419	211
39	573	716	643	418	209
39	570	710	636	412	205
37	563	698	623	402	200
35	553	681	605	389	193
31	540	660	584	374	185
25	524	634	558	356	175
18	504	604	528	335	164
09	482	571	496	314	153
01	461	539	465	293	143
95	442	510	436	274	133
91	426	483	409	255	123
90	412	458	382	236	114
90	399	433	356	218	104
90	387	409	331	201	96
91	378	388	309	186	88
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ECHELLOGRAM SUBSECTION

TAPE 255 - DESTRUCTIVE R/O SIMULATION (SEC ALCNE), SEC PSF WIDTH = 100 MICRONS

	TS:	201 125	TO 2	225 275			AL PI = 0.			400 S	UM =	0.111	.3E 08	3										
515	474	389	290	199	127	76	45	31	32	50	90	155	242	334	406	430	399	330	248	172	110	67	40	37
513	471	384	285	195	124	75	44	31	33	52	94	162	253	350	424	447	414	341	256	176	113	68	40	27 26
503	460	374	276	189	120	72	43	30	33	54	97	168	261	360	436	459	423	347	259	178	114	68	40	26
486	443	359	265	180	114	69	41	30	33	55	39	170	265	365	440	462	425	347	258	177	113	67	39	25
463	421 397	341 320	250 234	170 159	108	65	39 37	29	33	55	99	170	264	364	437	458	419	341	252	172	109	65	38	24
437 409	370	298	218	157	191 93	61 56	34	27 26	32 31	54 52	97 94	167 162	259 251	356 344	427 412	446 429	407 390	330 315	243 232	165 157	105 100	62 59	36 34	23 21
380	343	275	201	136	86	52	32	24	29	50	90	155	240	328	393	408	370	298	219	148	94	56	32	20
349	315	252.		124	78	47	29	22	28	47	85	146	226	310	370	383	347	279	204	138	87	52	30	19
318	285	228	165	111	70	42	26	21	26	44	80	136	211	288	343	355	320	257	187	127	80	48	27	18
286	256	204	147	99	62	38	23	19	24	40	73	125	194	264	315	325	292	234	170	115	72	43	25	16
255 226	228 202	181 160	131	88 78	55 49	34 30	21 19	17 15	21 19	37 33	67 60	114	176 159	240 217	285 257	294 265	264 238	211 190	. 153 138	103 93	65 58	38 35	22 20	15
199	178	141	102	68	43	26	16	13	17	30	55	93	144	196	233	240	215	172	125	84	53	32	19	14 13
175	156	123	88	59	37	22	14	12	16	27	49	85	130	178	212	218	196	157	114	77	49	29	iŕ	12
153	136	108	77	51	32	19	12	10	14	25	45	77	120	163	194	201	181	145	105	71	45	27	16	12
136	121	95	68	45	28	17	11	9	13	23	42	72	111	151	180	186	167	134	97	65	41	24	15	11
122 112	107	86 79	62 57	41 38	26 24	16 15	10	9 8	12	21 20	39 36	66 62	103 96	140 130	167 155	172 160	154 143	123	89	60	37	22	14	11
104	93	74	53	36	23	14	9	7	10	18	34	58	90	122	145	150	134	107	82 77	55 52	34 33	21 20	13 12	10
98	88	70	51	34	21	13	8	7	10	17	32	55	65	116	138	142	127	102	74	50	31	19	12	11
94	84	61	49	33	21	13	8	7	9	17	31	53	81	111	132	136	122	98	71	48	30	18	12	11
91	8.2	66	48	32	20	15	8	7	9	16	29	51	78	107	127	131	118	94	69	46	29	18	12	11
90 89	81 81	65 65	48	32 32	20	12	8	6	9	15	28	49	75	103	123	127	114	91	66	45	28	17	12	12
89	81	65	48 48	32	20 20	12	8 8	6 6	8 8	15 14	27 27	47 46	73 70	100 96	119 114	122 118	110 106	88 85	64 62	43 42	27 26	17 17	1 <i>2</i> 12	13 13
89	81	65	48	32	20	12	8	6	8	14	26	44	68	93	111	114	103	82	60	40	26	16	12	14
90	81	65	48	32	20	12	8	6	В	14	25	43	66	90	108	111	100	80	59	40	25	16	12	15
90	82	66	48	33	21	12	8	6	8	13	24	42	65	89	106	109	99	80	58	39	25	16	13	16
9 L 94	83 85	67 69	49 51	33 35	21 22	13 13	8	6	8 8	13 13	24	41	64	88	105	109	99	80	59	40	26	17	14	18
97	89	72	53	36	23	14	8 8	6 6	8	13	24 25	42 42	65 66	89 91	106 109	111 113	101 103	81 83	60 61	41 42	26 27	17 18	14 15	19 20
103	94	77	57	39	24	15	ÿ	7	8	14	25	44	68	93	111	116	106	85	63	43	28	18	16	22
110	101	82	61	42	26	16	9	7	8	14	26	45	69	95	114	119	109	88	65	44	29	19	17	23
119	110	90	67	46	29	17	10	7	9	15	27	46	72	99	118	124	113	92	68	46	30	20	18	25
132 148	122 136	100	75 84	5 L 5 B	33 37	19 22	11	В 9	9 10	15	28	48 51	75 79	103	124	129	118	96	71	49	32	21	19	26
166	154	127	94	65	41	24	14	10	11	16 17	29 31	54	84	109	131 138	137 145	125 133	102 108	75 80	52 55	34 36	23 24	20 21	27 28
188	174	143	106	73	46	27	16	11	11	18	33	57	89	123	147	154	142	116	86	59	38	25	22	29
212	195	160	119	82	52	31	18	12	13	20	36	62	96	132	159	167	153	125	93	64	41	27	23	30
237	218	179	133	91	58	34	20	13	14	22	40	68	105	144	173	181	166	136	101	69	45	29	24	31
263	242	198	147	100	64	38	22	15	15	25	44	75	115	157	189	197	180	147	109	75	48	32	25	31
290 317	266 290	217 237	161 175	110 120	70 75	41 45	24 26	16 18	17 19	27 30	48 53	82 89	126 136	171 186	205 221	214 231	195 211	159 172	118	81	52	34	26	32
344	314	256	189	129	81	48	28	19	20	32	57	96	147	200	238	248	226	184	127 136	87 93	56 60	36 38	27 29	32 32
369	337	273	202	137	86	51	30	20	22	34	61	103	157	213	254	264	241	196	144	98	63	40	30	33
391	356	288	212	144	90	53	31	21	23	36	64	109	166	226	269	280	255	206	152	104	66	42	30	33
409	371	300	220	149	94	55	32	22	24	38	68	115	175	238	283	294	267	216	159	108	69	43	31	33
422 431	382 389	308 312	225 228	152 154	96 96	56 57	33 34	23 24	25 26	40 42	71 75	120 126	184 191	249 258	295 306	306	277	224	164	111	71	45	32	33
434	391	313	228	153	96	57	34	24	27	44	78	130	191	265	314	316 323	286 291	230 234	168 171	114	73 74	46 46	32 32	33 33
433	388	310	225	151	94	56	33	24	28	45	79	133	201	270	318	326	294	235	172	116	74	46	32	33
																					-	_		

Figure A-3. Echellogram Subsection - Tape No. 255

426 415 401 384 365 343	381 370 357 340 322 302	303 294 282 269 253 237	219 212 203 193 182 169	147 142 136 129 121 112	92 89 85 80 75	54 53 50 48 45 42	33 31 30 29 27 26	24 23 23 22 21 20	28 27 27 26 26 25	45 45 45 44 43	80 80 79 77 75 74	133 133 131 126 124 121	202 200 197 192 186 181	270 268 263 256 248 239	318 315 308 299 289 278	326 322 314 304 293 281	293 288 281 271 261 249	234 230 223 215 206 197	170 167 162 155 149 142	115 112 109 104 100 95	73 71 69 66 63	46 45 43 42 40 39	32 32 31 31 30 30	33 33 33 33 33
321	282	220	157	104	65	39	24	19	25	42	72	118	175	231	266	268	237	186	134	89	57	37	29	34
300	262	204	145	96	60	36	22	19	24	41	71	115	169	221	254	254	223	175	125	83	53	35	26	35
279	243	189	134	88	55	33	21	18	24	40	69	111	162	210	239	239	209	163	116	77	50	33	28	36
259	225	174	123	81	50	30	19	17	23	39	67	106	154	198	224	223	194	151	107	71	46	31	28	37
241	208	160	113	74	46	28	18	16	22	38	64		146	186	210	207	179	139	99	66	42	29	27	39
225	193	148	104	68	. 42	25	17	15	21	37	62	97	138	175	196	192	166	128	90	60	39	28	27	40
212	181	138	97	63	39	23	16	15	21	36	60	94	132	165	183	178	152	117	82	55	36	26	28	43
201	170	129	90	58	36	22	15	14	21	35	59	91	126	156	171	164	140	107	75	49	33	25	28	45
191 183	160 152	121	84 79	54 51	33 31	20 19	14	14	21 20	35 35 34	58 57	88 85	121	147	159 148 138	152 140	128 117 107	97 88 80	68 61	45 41 37	30 27 25	24 23 22	28 29 29	47 49 51
177 176 177	147 145 145	110 108 107	76 74 73	49 48 47	30 29 28	18 18 17	13 12 12	13 13 13	20 20 20	34 34	56 55 54	83 81 79	111 106 103	131 125 126	130 124	129 120 113	99	74 69	56 51 48	34 32	24 22	21 21	29 29 30	53 54
181	147	108	74	47	28	17	12	13	20	34	55	79	103	119	121	110	90	67	46	31	22	21	30	56
186	150	110	74	47	28	17	12	13	21	35	57	82	106	121	122	110	90	66	46	30	22	21	31	56
194	155	112	75	47	28	17	12	14	22	38	60	86	110	125	125	112	90	66	45	30	21	21	31	57
204	161	117	78	48	29 .	17	13	15	24	40	64	91	116	130	129	114	93	66	45	30	21	20	31	57
218	171		82	50	30	18	13	16	26	43	69	98	123	137	134	118	91	67	45	30	21	20	30	56
235	184	131	87	53	31	19	14	17	28	47	74	105	131	145	141	122	96	69	46	30	21	20	30	56
255	198	141	93	57	33	20	15	18	30	51	80	113	141	154	149	128	100	71	47	30	21	20	30	55
277	214	152	99	60	35	21	16	20	33	56	87	123	152	165	158	136	105	75	49	32	22	20	29	54
299	230	162	105	64	37	22	17	22	36	6 L	95	133	164	178	169	144	111	79	52	33	22	20	29	52
321	245	172	111	67	39	23	18	23	39		104	145	178	191	182	154	118	83	54	34	23	20	28	50
343	261	182	117	71	41	24	19	25	42	72	112	157	192	206	194	163	125	87	57	35	23	20	27	48
365	276	192	124	74	43	26	21	21	46	78	122	169	207	221	207	173	132	92	60	37	24	20	26	46
385	290	202	130	78	45	27	22	29	49	84	131	181	221	235	220	183	138	96	62	38	24	20	25	44
402	302	209	134	80	46	28	23	31	53	89	139	193	234	248	232	192	145	101	65	40	25	20	24	41
413	309	213	136	82	47	28	24	33	55	94	146	203	246	260	242	200	150	104	67	41	25	19	23	39
417 417 411	312 310 304	214 212 208	137 135 132	82 80 79	47 46 45	29 29 28	25 25 25	34 35 36	58 60 62	98 102 105	153 158 163	211 219 225	256 265 271	271 279 286	251 258 263	207 213 216	155 159 160	107 109 110	69 70 70	42 42 42	26 26 25	19 18 18	21 19	36 33 31
401 388 374	296 287 275	202 195 187	128 124 119	77 74 71	44 43 41	28 27 26	25 25 25	36 36 36	63 63 62	107 107 106	166 166 164	228 228 225	275 274 270	288 286 281	264 261 255	215 212 207	159 156 152	109 106 103	69 67	41 40 39	25 24	17 16 15	16	28 26
357 338	262 248	178 168	113 106	67 63	39 37	25 24	24 23	35 34	61 59	104 100	160 154	219 211	262 252	272 261	247 237	199 191	146 140	99 95	65 63 60	37 36	23 22 21	15 14	16 15 14	24 22 21
317	232	157	99	59	34	22	22	32	56	95	147	201	240	249	225	181	133	90	57	34	20	13	13	20
296	217	146	92	55	32	21	20	30	53	90	139	190	227	236	213	172	126	85	54	32	19	13	12	19
275	201	135	85	51	30	19	19	29	50	85	131	180	214	222	201	162	118	80	51	30	18	12	12	18
254	185	124	78	46	2 <i>1</i>	18	18	27	47	80	123	169	201	208	188	152	111	75	48	28	17	11	11	18
233	169	114	72	43	25	17	17	25	44	75	115	157	188	194	175	141	103	70	44	26	15	11	11	17
213	155	104	66	39	23	15	15	23	41	69	107	146	174	179	162	129	94	63	40	24	14	10	11	17
196	142	96	60	36	21	14	14	21	38	64	98	133	158	163	146	117	84	56	35	21	12	9	10	17
179	130	87	55	33	19	13	13	19	34	58	88	120	143	146	130	103	74	49	31	18	11	8	10	16
164	119	60	50	30	17	11	11	17	31	51	79	107	127	130	115	91	65	43	27	16	10	7	9	16
151	109	73	46	27	16	10	10	16	27	46	70	95	112	114	101	80	57	38	23	14	9	7		16
140	101	63	42	25	14	9	9	14	24	41	62	84	99	101	90	70	50	33	21	12	8	7		16
131 125	95 90	64 61	40 38	23 22	13 13	9	8	12 11	21 19	36 32	55 50	75 67	88 79	90 81	80 72	63 57	45 41	30 27	19 17	11 10	7 7	6	9 9	17 17
119 115 111	86 83 80	58 56 54	36 35 34	21 21 20	12 12 11	8 7 7	7 7 6	10 9 9	17 16 15	29 27 26	45 42 40	61 57 54	73 68 64	75 70 66	67 63 60	53 50 48	38 36 35	26 24 23	16 15 15	10 9 9	6 6 6	6 6	9 10 10	18 18 19
107 104 102	78 76 74	53 51 50	33 32 31	19 19 18	11 11 10	7 7 6	6 6 6	9 8 8	15 14 14	25 24 24	38 37 37	52 51 51	62 61 60	64 63 63	58 57 57	46 46 46	34 33 33	23 23 23	14 14 14	9	6 6 7	7 7 7	11 12 13	21 22 24
100 99	73 72	49 49	31 31	18 18	10	6	6 6	8 8	14 14	24 24	37 37	51 51	60 61	63 63	57 57	46 46	34 34	23 23	15 15	9	7 7	8 8	13 14	26 27
100 102 104	73 75 77	49 50 52	3 _/ î 32 33	18 19 19	10 11 11	6 7 7	6 6	8 9	14 15 15	24 25 26	38 38 40	52 53 54	62 63 65	64 66 68	58 60 62	47 49 50	35 36 37	24 24 25	15 16 16	01 01 10	7 8 8	9	15 15 16	28 30 31
								Fi	gur	e A-	3 (Shee	et 2	of	6)									

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EK-26

TAPE 255 - DESTRUCTIVE RIO SIMULATION (SEC ALCNE). SEC PSF WIDTH # 100 MICRONS

ECHELLOGRAM SUBSECTION

	PTS: 226 TO 250 RECS: 125 TO 275					TOTAL PIXELS = 102400 SUM = 0.1113E 08 AVG = 0.1087E 03																		
27	41	71	121	186	254	302	312	280	224	163	109	69	41	24	17 17	18 19	29 32	51 56	66 93	130 141	174 190	205 223	211 229	191 207
25	33	66	111	171 157	233 215	277 255	286 263	257 237	206 189	149 138	101 93	63 58	38 35	23 21	16	20	34	61	101	153	205	241	247	223
24 23	35 33	51 56	94	145	198	236	243	218	174	127	85	54	32	20	16	21	36	65	109	165	220	258	264	237
21	30	52	87	134	183	218	224	202	161	117	78	49	30	19	16	22	39	70	116	175	233	272	277	249
20	28	48	81	125	170	202	209	187	149	108	73	46	28	18	16	23	41	73	121	182	242	282	287	256
19	27	45	76	117	163	190	196	176	140	102	68	43	26	17	16	23 23	42 42	75 76	124 126	186 188	248 250	288 290	292 294	260 261
18	25	43	72	111	151 146	180 174	186 179	167 162	133 129	97 94	65 63	41 40	25 25	17 16	16 16	23	42	76	126	188	249	289	293	260
17 16	24 23	41 40	69 68	107 104	142	170	176	159	127	93	63	40	24	16	16	23	42	75	125	187	247	287	289	257
15	23	39	67	103	141	168	175	158	128	93	63	40	25	16	16	23	41	74	123	184	244	282	285	253
15	22	39	67	103	141	1 69	176	160	129	95	64	41	25	17	16	23	41	73	121	181	240	277	280	248
14	22	40	68	105	143	172	178	162	131	96	65	41	25	17	16	23	40	72	119	178	235	272	274	243
14	22	40	69	106	146	175	182	165	134	98	67	42	26	1.7	16 16	22 22	40 40	71 70	117	175 172	239 226	266 261	268 262	238 232
14	23	41	76	109 112	149 153	178 184	186 192	169 175	137 142	101 104	68 71	44 45	27 27	17 18	16	23	40	70	115	170	223	256	25ŏ	227
14 14	23 24	42 43	72 74	115	158	190	198	181	147	104	73	47	28	18	16	23	40	70	114	167	218	249	249	219
14	24	45	77	119	164	197	205	187	152	112	76	48	29	19	17	23	40	70	112	164	212	241	240	210
14	25	46	80	124	171	205	214	195	158	116	79	50	31	20	17	23	40	68	110	159	205	231	229	200
14	25	49	84	130	179	215	224	205	166	123	83	53	32	21	18	23	39	67	106	153	196	220	216	189
15	28	52	89	138	189	227	237	217	176	130	89	56	34	22	18	23 23	38 38	65 63	103	147 141	186 177	208 197	204 192	177 166
16	30	56	96	148	203	243 262	254 274	232 250	189 204	140 151	95 103	60 65	37 39	23 24	19 19	23	38	62	97	136	169	187	181	156
18 19	33 36	61 66	104	161 175	219 238	284	297	272	222	164	112	71	43	26	20	24	38	62	95	131	162	177	171	146
21	39	13	124	191	260	310	324	296	242	179	122	78	47	28	21	25	38	61	93	128	157	170	162	138
22	43	80	136	209	285	340	355	325	265	197	134	85	51	31	23	25	38	61	92	126	152	163	154	131
25	47	88	150	230	313	373	390	357	292	216	148	94	56	34	24	26	39	62	92	124	148	157	148	125
27	52	97	166	254	344	411	429	393	321	238	163	103	62 67	37 40	26 28	28 29	40 42	63 65	93 94	123 124	146 145	153 151	143 139	119 115
29	57	107 117	182 200	279 306	379 415	452 495	471 516	432 472	352 385	261 285	178 194	113	73	43	30	31	44	68	97	127	147	150	137	113
32 35	63 69	126	218	333	452	538	560	512	416	308	210	132	79	47	33	33	47	72	103	132	151	153	139	113
38	75	139	236	360	488	581	603	550	447	330	224	142	84	50	35	36	51	77	110	140	158	159	142	115
41	80	149	253	386	523	621	644	586	476	350	238	150	89	53	38	39	55	84	118	150	168	167	148	119
43	85	158	269	410	555	658	682	650	502	369	250	158	94	56	40	42	60	91 99	128 139	161 173	179 192	176 187	155 163	124 129
46	90	167	283	432	584	69l	715 743	649 673	524 543	385 398	261 269	164 170	98 101	59 61	43 45	46 50	66 72	108	151	188	204	199	173	135
48 50	94 98	175 181	296 307	451 466	608 628	720 743	765	692	556	407	275	173	104	63	48	54	78	118	164	203	221	213	183	142
52	Let	186	315	478	643	758	780	763	564	411	277	175	105	65	50	58	85	128	178	219	237	227	193	149
53	103	190	319	484	650	765	785	706	565	411	277	174	105	65	52	62	92	139	192	235	253	240	203	156
54	104	191	321	485	650	764	782	701	560	407	273	172	104	66	54	65	99	149	206	251	269	253	213	162
54	104	191	319	482	644	755	771	689	549	398	267	168	102	65	55 56	69 72	105 111	159 168	219 231	266 280	283 297	265 277	222 231	168 174
55	104	189	315	474	632	739 716	752 727	671 647	533 512	385 369	258 247	162 155	99 95	64 63	57	75	117	177	243	294	311	289	239	180
54 54	103	186 181	309 300	463 448	593	689	697	618	487	350	234	147	90	61	57	78	122	186	255	308	324	300	248	186
53	99	176	291	431	568	657	662	585	460	330	220	139	86	59	57	80	127	194	265	320	336	310	255	190
53	96	171	280	413	541	623	626	551	432	309	206	130	81	57	57	82	131	200	274	329	345	317	260	193
52	94	165	269	394	514	588	589	516	404	Z89	192	121	76	55	57	83	134	204	280	336	351	321	262	194
51	92	160	258	376	487	554	552	482	376	268	178	112	71	52	56 55	84	135	206 205	282 279	337 333	351 346	320 314	260 254	192 186
51	90	155	248 238	358 341	460 434	529 487	515 480	448 415	349 322	247 228	164 150	103 95	66 61	50 47	53	83 80	134 131	200	272	324	335	303	244	178
50 49	88 86	150 146	229	324	410	456	446	385	297	210	138	87	56	44	50	77	126	192	260	310	320	288	231	168
49	84	142	221	311	388	429	417	357	275	193	127	80	51	40	47	73	119		246		301	270	216	157

Figure A-3 (Sheet 4 of 6)

49	84	140	216	300	271	6.D6	201	333	266	170	117	74	47	37	44	68	111	170	230	273	280	251	199	L45
49	84	140	213	292	357	386	368	312	237	166	108	68	44	34	41	63	103	157	213	252	258	231	183	133
50 51	85 86	140 141	211 210	286 281	345 335	368 353	348 331	293 276	221	154 144	100 93	62 58	40 37	32 29	37 34	58 53	95 87	144 133	196 180	231 213	237 218	212 195	169 155	122 113
52	88	142		278	327	342	317	262	196	135	87	54	34	27	32	49	80	122	165	196	201	179	143	104
53 54	90 93	145				334	307	252	188	129	83	51	32	25	29	45	74	112	152	180	184	165	131	95
56	96	154	216	281 286	323 326	330 329	300 296	244 240	181 176	123 120	79 76	48 46	30 28	23 22	27 25	41 38	68 62	103 94	139 127	164 150	168 153	150 137	119 108	86 78
59	101	161	231	295	333	333	297	239	175	118	74	45	27	20	23	35	57	86	116	137	140	124	98	70
62 66	107	170 181	243 257	308 324	344 360	341 354	302 310	241 245	175 177	118 118	74 74	44 44	27 26	19 18	21 20	32 29	52 47	78 72	106 97	125 114	127 116	113	89 81	64 58
71	122	193	274	342	377	368	320	251	180	119	74	43	25	18	18	27	43	66	89	105	107	95	75	54
76	131	206	291	362	396	383	330	257	183	120	74	43	25	17	17	25	40	61	82	96	98	87	69	49
80 85	139 147	219 232	308 325	381 400	414 432	397 411	339 348	262 267	186 188	121 122	74 74	43 42	24 24	16 16	16 15	23 22	37 34	56 52	76 70	89 83	91 84	81 75	64 59	46 43
90	155	244	340	417	448	423	357	272	190	123	74	42	24	15	14	20	32	49	66	77	79	71	56	41
94 98	163 169	255 265	355 368	434 448	463 477	435 446	364 371	276 280	193 195	124	75 75	42	23	15	14	19	30	46	62	73	75	67	53	39
101	175	273	379	460	488	454	376		195	125 125	75	42 42	23 23	14 14	13 13	18 18	29 28	44 43	59 58	70 69	72 71	65 64	52 51	37 37
103	179	279	386	468	494	458	377	282	195	124	74	41	23	14	13	10	28	42	57	68	71	64	51	38
105 105	181 182	282 283	390 391	471 472	496 496		376 374	281 278	193 191	123	73 72	41 40	22	14 14	13	18 -18	28	43	58	70 72	72 75	66	53	39
105	182	283	390	470	493	453	370	275	188	120	71	39	22 22	14	13 13	19	29 31	44 47	61 64	76	79	69 72	56 59	41 43
105	181	281	387	466	488	448	365	271	185	117	69	39	21	14	14	20	32	49	67	80	83	76	62	45
104 102	179 176	278 273	383 376		481 471	440 429	358 348	265 257	181 175	114 111	68 65	36 36	21 20	14 14	14 14	21 22	34 35	52 54	71 74	84 89	88 92	80 84	65	48 50
100	172	266	366	438	457	416	336	248	168	106	63	35	20	13	15	23	37	57	78	93	97	89	68 72	50 53
96	166	257	353	423	440	400	323	238	161	102	60	34	19	13	15	24	39	60	83	99	103	94	76	56
93 89	160 152	247 236	339 324	406 387	422 403	383 365	309 295	227 217	155 147	98 93	58 55	32 31	19 18	14 14	16 17	25 27	42 45	64 70	88 96	106 115	110 120	101	82 90	61 67
84	145	224	308	368	382	346	279	205	139	88	52	29	17	14	18	30	50	77	105	126	133	122	100	74
80 75	137 128	212 198	299	346	359	325	262	191	130	82	48	28	17	14	19	33	55	85	117	141	147	135	111	82
70	119	184	271 251	323 299	335 309	302 278	243 223	177 162	120 109	75 69	45 41	26 24	16 16	15 15	21 24	37 41	62 70	96 107	131 146	157 174	164 182	150 166	123 135	91 100
64	110	169	231	275	284	255	204	148	100	63	37	22	15	16	26	46	78	119	161	192	200	183	149	110
59 54	101	155 143	212 195	252 232	260 239	234 215	187 172	136 125	92 84	58 53	35	21	15	17	28	51	B6	131	178	211	220	201	163	121
50	85	131	179	213	220	198	158	115	77	49	32 29	20 18	15 15	18 19	3 I 3 3	56 60	94 102	143 156	194 212	231 252	240 262	219 239	179 194	132 143
46	78	121	165	196	202		144	104	70	44	27	17	14	20	36	65	111	169	230	273	283	258	210	155
43 39	72 67	11 L 102	151 139	180 166	185 170	166 152	132 121	95 87	64 59	40 37	24 22	16 15	14 14	21 22	38 41	70 76	119 128	183 196	248 266	294 316	305 327	278 298	225 241	166 177
37	62	95	130	155	159	143	114	82	55	35	21	15	15	23	44	18	138	210	285	338	349	317	256	188
35 33	59 56	90 87	123 118	147 141	151 145	136 131	108 105	79 76	53 51	33	21	15	15	25	47	87 92	147	224	302	358	369	334	270	198
32	54	84	115	137	141	127	102	74	20	33 32	20 20	15 15	16 16	26 27	50 52	96	155 162	236 247	318 333	376 393	388 404	351 365	283 294	207 215
31	53	82	112		138		100	73	49	31	20	15	17	29	54	100	169	257	346	408	420	378	304	222
30 30	52 51	80 79	110	131 129	135 134	122	98 98	72 71	49 48	31 31	20 20	15 15	17 18	30 31	56 58	104 107	175 180	266 213	357 366	421 430	432	369	312	228
30	5 L	79	108	129	134	121	98	71	48	31	20	15	18	31	60	109	184	277	371	435	441 444	396 398	316 317	230 230
3C	51	79	108	129	134	122	98	72	49	31	20	15	19	32	61	111	185	279	372	435	443	395	314	227
30 30	51 51	79 80	108 109	130 131	135 136	122	98 100	72 73	49 50	31 32	20 21	16 16	19 19	32 32	61 61	111	185 183	277 274	369 364	430 423	437 428	389 380	308 300	223 216
30	52	81	111	133	138	126	102	15	51	33	21	16	19	33	61	110	181	270	356	412	416	368	290	208
31 32	53 55	83 85	113	136 140	142 146	129 133	104 108	77	52	34	55	1.7	19	33	61	109	178	264	347	399	401	354	278	199
33	57	88	121	146	152	139	113	80 83	54 57	35 36	22 23	17 18	50 50	33 33	60 60	107 105	175 170	257 249	335 322	384 367	385 366	338 320	264 250	189 178
34	59	92	127	152	159	145	118	87	59	38	24	Įŝ	20	33	59	103	166	240	309	350	347	302	235	167
36 39	63 67	98 104	134 142	161 170	168 178	153 162	125 132	92 97	63 66	46 42	26 27	19 20	21 21	33 33	58 58	101	161 158	232 225	296	334	329	286	222	157
42	72	111	151	181	188	171	139	102	70	45	28	20	22	33	59	100	156	220	285 276	319 306	313 298	270 256	209 197	148 138
45	77	118	160	191	198	180	146	107	73	47	30	21	22	34	59	100	155	215	268	293	283	242	185	130
48 50	81 85	125 131	169 177	201 210	208 218	189 198	153 160	112 118	77 80	49 51	31 32	22 23	23 24	35 36	60 62	101 102	154 154	212 209	260 253	282 272	270 258	229 217	174	122
53	89	137	185	220	228	207	168	124	84	54	34	24	25	37	63	103	154	207	248	264	247	207	156	114 108
55 58	94 98	143 151	194 205	231 243	240 253	218 230	177 187	130 138	89 94	57 60	36	25	26	39	65	105	156	207	245	257	239	199	149	103
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ECHFLLOGRAM SUBSECTION

TAPE 422 - DESTRUCTIVE R/O SIMULATION(COMPLETE SYSTEM), LAMBDA = 2000 ANGST, SEC PSF WIDTH = 50 MICRONS

	TS: ECS:	201 TO 225 : 125 TO 275						XELS -		400 SI	um =	0.109	8E 08											
374	371				135	100	78	68	66	71	86	113	156	211	267	301	299	263	209	157	116	88	72	66
387	383	333	261	19 L	137	101	80	69	67	73	89	118	164	223	282	318	315	275	218	162	119	90	73	65 65
395	394	339	264	193	138	101	80	70	68	74	91	122	171	233	295	333	329	287	226	167	122	91 92	73 73	65 64
398	392	339	264	192	138	101	80	70	69	76	93	126	177	242	307	346 356	342 350	297 304	233 237	171 174	124 125	93	73	64
395	389 389	335 328	261 255	190 185	136 133	100 99	80 79	70 69	69 69	76 77	95 95	128 130	181 184	249 253	316 321	361	355	307	239	174	125	92	73	63
387 375	368	317	246	179	129	96	77	68	68	76	95	130	184	253	321	361	355	306	238	173	124	91	72	62
360	352	303	236	172	124	93	75	67	67	75	94	129	182	251	318	357	350	301	234	170	122	90	71	60
341	334	288	224	164	119	89	73	65	66	74	92	126	178	245	310	348	341	293	227	165	119	87	69	59
322	315	271	211	155	113	86	70	63	64	72	90	123	173	237	300	336	328	282	219	160	115	85	67	58
300	294	253	197	145	106	81	67	61	62	7 C	87	118	166	227	286	321	313	269	209	153	110	82	65	56
278	272	234	183	1 35	100	77	64	59	60	67	84	113	i 58	215	271	303	296	254	197	145	105	79	63	55
256	250	215	169	125	93	73	61	56	57	64	80	107	149	202	254	263	276	237	185	136	100	75	61	53
234	228	197	154	116	87	68	58	54	55	62	76	101	139	188	235	262	256	220	172	128	94	72	58	52
212	297	179	141	106	81	64	55	51	52	59	72	95	130	174	217	242	236	203	160	119	88	66 65	56 54	50 49
192	187	162	128	98	75	6C	52	49	50	56 53	68	89 83	121	161	200 185	22 <i>2</i> 205	217 200	187 173	148 137	111 104	83 79	62	52	48
173	168 152	146 132	116 106	89 82	69 64	56 53	49 47	47 44	48 46	51	64 61	78	113 105	149 139	171	190	185	161	128	97	74	59	51	47
156 141	137	120	96	75	59	50	44	42	44	48	58	74	99	130	160	176	172	150	120	92	71	57	49	46
129	125	110	89	70	56	47	42	41	42	46	55	70	93	122	149	165	161	140	112	86	67	55	48	45
119	116	101	82	65	52	45	40	39	40	44	53	67	88	115	140	155	151	132	106	82	64	53	47	45
111	108	95	77	62	50	43	39	38	39	43	50	64	84	109	133	146	143	124	100	78	62	52	46	45
105	102	90	74	59	48	41	37	36	38	41	49	61	86	104	126	139	136	118	96	75	60	51	46	45
100	98	86	71	57	46	40	36	35	37	40	47	59	77	99	121	133	130	114	92	73	58	50	46	45
97	95	83	69	55	45	39	36	35	36	39	46	57	74	96	117	128	125	110	89	71	57	49	46	46
95	92	82	67	54	44	38	35	34	35	30	45	56	72	93	113	124	121	107	87	69	57	49	46	47
94	91	80	66	53	44	38	35	34	34	38	44	54	70	90	110	121	110	104	85	68	56	49	47	48
93	91	80	66	53	43	37	34	33	34	37	43	53	69	88	107	117	115	101	83 82	67 66	56 56	49 50	47 48	49 50
93 93	91 91	80 80	66 66	53 53	43 43	37 37	34 34	33 33	34 34	37 37	42 42	52 52	67 66	86 85	104	114	112	98	81	66	56	50	49	52
94	92	81	66	53	44	38	34	33	34	36	42	51	66	84	101	111	109	97	80	66	56	51	50	53
95	93	82	67	54	44	36	35	33	34	37	42	51	65	83	100	110	108	97	18	66	57	52	51	55
97	95	84	69	55	45	39	35	34	34	37	42	52	66	84	101	111	109	97	81	67	57	53	53	57
100	98	86	71	57	46	39	36	34	35	37	43	52	66	84	102	112	110	99	82	68	59	54	54	59
104	102	90	74	59	48	41	37	35	35	38	43	53	67	86	104	114	113	100	84	69	60	55	56	61
109	107	94	77	6 i	50	42	38	36	36	39	44	54	69	88	106	117	115	103	86	71	61	57	57	63
116	113	100	82	65	52	44	39	37	37	40	45	55	71	90	109	120	119	106	88	73	63	58	59	64
125	122	107	87	69	55	46	40	38	38	41	47	57	73	93	113	124	123	109	91	75 70	64	60	60	66
135	132	116	94 102	74 79	58 62	48 50	42 44	39 41	39 41	42 43	48 50	59 61	76 79	97 101	118	130 136	128 134	114	95 99	87 1B	66 68	61 63	62 63	68 69
148 163	145 159	127 138	111	85	66	53	46	42	42	45	52	6+	83	106	129	143	141	125	103	84	71	64	64	70
179	174	152	121	92	70	56	48	44	44	47	54	67	87	112	137	151	149	132	108	88	73	66	66	71
197	191	166	131	99	75	59	50	46	46	49	57	71	92	119	146	161	158	139	114	92	76	68	67	72
215	209	181	143	107	80	63	53	48	47	51	59	75	98	127	156	172	168	148	121	96	79	70	68	73
234	228	196	154	115	85	66	55	50	49	53	62	79	104	136	166	183	179	157	127	100	82	71	69	74
254	246	212	165	122	90	7 C	58	52	51	55	65	83	110	145	177	195	191	167	134	105	85	73	70	74
273	265	227	176	130	95	73	60	54	53	57	68	87	117	153	188	208	203	176	141	110	87	75	71	74
291	282	241	187	137	100	76	62	56	55	59	71	91	123	162	199	220	214	186	1 4B	114	90	76	71	74
308	298	254	197	143	104	79	64	57	56	61	73	95	128	170	209	231	225	195	155	119	93	78	72	74
323	312	266	205	149	108	81	66	59	58 59	63	76	99	134	178	219	242	235	203	161	122	95 97	79 BO	72	74 74
334 343	323 331	274 281	211 215	153 156	110	83 84	67 68	60 61	60	65 66	78 80	102 105	139 143	185 191	228 235	251 259	244 251	210 216	166 170	125 128	98	80	73 73	74
243	2 2 L	501	4.13	170		0.4	40	2.5	30	30	30	100	. 43	1 71	633	277	201	510	110	120	70	00		, 4

Figure A-4. Echellogram Subsection - Tape No. 422

334 322 216 58 113 85 69 62 62 62 68 83 110 151 200 247 271 222 224 173 131 99 61 72 72 327 328 227 17 212 134 114 11 84 68 68 23 110 131 200 247 277 281 222 215 187 132 99 60 72 72 73 328 310 262 200 146 108 61 67 60 61 67 62 61 67 72 108 127 174 175 175 175 175 175 175 175 175 175 175	348 349	335 336	284 284	217 218	157 157	113	85 85	69 69	61 62	61 61	67 68	82 83	108 109	147 149	195 199	241 245	265 269	257 260	220 223	173 174	130 131	99 99	81 81	73 73	73 73
322 210 207 150 100 22 48 6 11 64 68 83 110 149 180 243 267 257 219 171 128 97 77 71 71 71 71 72 21 31 31 72 21 72 21 71 128 97 77 71 71 71 72 21 23 21 72 22 21 71 71 28 71 72 72 72 72 72 72 72 72 72 72 72 72 72	347	334	282	216	156	113	85	69	62	62	68	63	110	151	200	247	271	262	224	175	131				72
124 10																									
296 284 239 186 135 95 76 64 58 59 66 80 105 142 186 227 246 235 202 158 119 91 75 69 70 264 269 272 115 128 95 74 62 57 88 59 66 80 105 142 186 227 246 235 202 158 119 91 75 69 70 264 269 272 115 128 18 95 74 60 25 57 88 57 91 103 139 1816 219 238 227 187 182 182 183 183 183 183 183 183 183 183 183 183																	261		215		126	96	78	70	70
289 227 175 128 95 74 62 57 58 65 79 103 139 181 219 238 227 194 125 115 89 74 68 65 69 224 227 124 165 122 91 71 60 55 65 76 87 81 101 135 176 121 228 218 185 145 111 86 72 67 69 24 22 22 218 11 10 61 86 72 67 69 24 22 218 11 10 61 86 72 67 69 24 22 218 11 10 61 86 72 67 69 24 22 218 11 10 61 86 72 67 69 24 22 218 11 10 61 86 72 67 69 24 22 218 11 10 61 86 72 67 69 24 22 218 11 10 61 86 72 67 69 24 22 218 11 10 61 86 72 67 69 24 22 218 11 10 61 86 72 67 69 24 22 218 11 10 61 86 72 67 69 24 22 218 11 10 61 86 72 67 69 24 22 218 11 10 61 87 12 218 12																									
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226 212 178 138 103 79 63 55 52 53 60 73 94 123 150 184 195 185 157 125 97 78 68 65 70 214 199 167 130 93 75 61 53 51 52 59 71 92 119 150 184 174 148 118 92 75 66 65 70 203 188 157 123 93 76 25 55 52 98 71 89 115 144 168 118 92 75 66 65 70 203 188 157 123 93 76 25 52 40 51 58 70 89 115 144 168 118 92 75 66 66 77 203 188 157 123 93 76 25 52 40 51 58 70 89 115 144 168 118 92 75 66 66 77 204 180 157 123 93 76 25 52 40 51 58 70 89 115 144 168 118 92 75 66 66 77 205 180 157 123 93 77 6 15 15 14 14 14 14 14 14 14 14 14 14 14 14 14																									
24 199 167 130 93 75 61 53 51 52 59 71 92 119 150 175 184 174 148 118 92 75 60 65 70					_																	-			
178 149 116 89 69 57 50 48 50 57 69 87 112 138 158 164 153 130 104 83 70 63 64 71	214	199	167	130	99	75	61	53	51	52	59	71	92	119	150	175	184	174	148	118	92	75	66	65	70
186 170 141 110 85 66 55 49 47 49 56 68 86 109 133 150 154 143 122 98 79 67 62 64 72 180 163 135 106 81 64 54 48 47 49 55 67 84 106 128 143 143 122 93 76 65 61 63 73 176 159 130 102 79 63 53 47 46 48 54 66 83 103 123 136 138 126 107 88 72 63 60 63 73 177 175 1																									
180 183 135 106 81 64 54 48 47 49 55 67 84 106 128 143 146 134 114 93 76 65 61 63 73 176 156 130 102 79 63 53 47 46 48 54 66 83 103 123 136 132 107 188 67 60 63 73 173 154 127 77 75 16 57 47 46 48 54 65 82 101 120 131 131 119 107 83 67 65 60 63 73 177 158 122 77 75 60 51 46 45 48 54 65 82 101 120 131 131 119 107 83 67 65 59 63 74 179 159 126 77 75 60 51 46 45 48 54 65 82 101 120 131 131 119 107 83 67 65 58 63 73 179 159 126 77 75 60 51 46 45 48 54 65 82 101 120 131 131 119 107 83 67 65 58 63 73 179 159 126 77 75 60 51 46 45 48 54 65 82 101 116 123 120 107 91 75 64 56 58 63 73 184 153 126 77 75 60 51 47 47 50 57 70 87 107 122 127 121 107 89 73 63 57 57 62 75 192 163 127 79 76 61 52 47 47 50 57 70 87 107 122 127 121 107 89 73 63 57 57 62 75 192 163 127 99 76 61 52 47 47 50 50 48 48 54 59 77 87 107 122 127 121 107 89 73 63 57 57 62 75 192 163 127 99 76 61 52 47 47 50 50 48 48 59 77 87 107 122 127 121 107 89 73 63 57 57 62 75 192 163 183 164 183 164 183 164 183 164 183 164 183 164 183 164 183 164 183 164 183 164 183 164 183 164 183 164 183 164 183 164 183 164 183 183 164 183																									
173 154 127 99 77 61 52 47 46 48 54 65 82 101 120 131 131 119 101 83 69 62 59 63 74 175 153 126 97 75 60 51 46 45 48 54 65 81 100 110 124 122 110 93 77 65 59 58 63 75 179 155 126 97 75 60 51 46 45 48 54 65 81 100 110 124 122 110 93 77 65 59 58 63 75 186 137 125 97 75 60 51 46 45 48 55 66 82 101 116 123 120 107 91 75 64 58 58 63 75 186 137 129 97 75 60 51 46 45 48 55 65 68 82 101 116 123 120 107 91 75 64 58 58 63 75 186 137 129 97 75 60 51 46 45 48 55 65 68 84 103 116 123 120 107 91 75 64 58 58 63 75 186 137 129 137 138 104 80 63 54 49 49 52 61 76 95 116 132 136 127 107 89 73 62 57 57 62 75 214 178 138 104 80 63 54 49 49 52 61 76 95 116 132 136 127 107 89 73 62 57 57 66 27 224 189 152 113 85 67 56 52 51 56 66 83 106 130 146 148 130 112 91 74 62 57 56 62 74 149 152 113 88 67 56 52 51 56 66 83 106 130 146 148 130 115 93 74 62 57 56 61 73 244 199 152 113 88 67 56 52 51 56 66 83 106 130 146 148 130 115 93 74 62 57 56 61 73 248 223 187 122 91 71 59 54 54 60 72 92 119 146 164 165 149 123 98 77 66 3 77 56 60 71 278 223 187 122 91 71 59 54 54 60 72 92 119 146 164 165 149 123 98 77 64 57 55 59 70 334 259 190 115 97 78 62 58 68 59 60 68 85 114 114 124 124 125 107 89 76 63 77 56 60 71 348 259 190 115 97 78 62 58 67 66 82 107 130 174 124 124 125 107 89 77 66 3 77 56 60 71 348 259 190 115 97 78 62 58 67 67 62 62 77 97 126 155 174 174 148 130 112 91 86 67 57 55 59 70 348 259 190 115 97 78 62 58 67 67 62 62 77 97 126 155 174 174 149 130 114 180 107 82 66 57 54 59 60 354 284 296 145 105 80 67 62 63 78 98 68 82 107 130 174 149 193 111 188 107 82 65 57 55 60 365 284 296 145 105 80 67 62 63 78 98 68 87 112 137 159 156 16 87 149 149 149 149 149 149 149 149 149 149												67													73
173 153 125 97 75 60 51 66 45 48 54 65 81 100 111 127 127 125 114 97 80 67 60 59 63 75 175 175 155 125 97 75 60 51 46 45 48 54 65 81 100 116 124 122 110 93 17 65 95 86 37 75 179 179 155 125 97 75 60 51 46 45 48 55 66 82 101 116 123 120 107 91 75 64 55 86 63 75 179 179 179 179 179 179 179 179 179 179						_																			
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Figure A-4 (Sheet 2 of 6)

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4Q

ECHELLOGRAM SUBSECTION

YAPE 422 - DESTRUCTIVE R/U SIMULATIONICOMPLETE SYSTEM), LAMBDA = 2000 ANGST, SEC PSF WIDTH = 50 MICRONS

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86 109 149 212 301 407 502 548 522 437 331 236 168 124 101 92 96 115 149 195 240 263 252 212 160 86 108 146 207 293 393 482 524 498 417 316 226 162 121 99 91 97 116 152 200 246 270 259 216 162 85 106 143 202 283 378 461 498 472 395 300 216 155 117 96 90 96 117 154 203 250 275 263 219 164 84 105 140 196 274 363 439 472 446 373 283 204 148 112 94 88 95 117 155 204 252 277 264 219 164 83 103 138 191 264 347 417 446 420 351 267 193 141 108 91 86 94 116 154 203 251 275 262 217 162																		111	141	182					
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85 106 143 202 283 378 461 498 472 395 300 216 155 117 96 90 96 117 154 203 250 275 263 219 164 84 105 140 196 274 363 439 472 446 373 283 204 148 112 94 88 95 117 155 204 252 277 264 219 164 83 103 138 191 264 347 417 446 420 351 267 193 141 108 91 86 94 116 154 203 251 275 262 217 162		-																							
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Figure A-4 (Sheet 4 of 6)

82	100	132	181	247	318	376	396	370	307	234	171	126	98	84	81	90		147		240			206	153
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79	97	127	171	228	285	326	335	306	253	193	143	107	85	74	73	60	98	129	169	206	224	213	176	132
79 79	96 96	126 126	170 169	224 221	277 271	313 303	318 305	289 274	238 224	181 171	134 127	102 97	8 L 7 B	71 68	70 67	76 73	93 89	12Z 115	159 149	193 180	210 196	199 186	165 155	124 117
78	96	126	169		207	295	293	262	213	162	121	92	74	66	64	70	84	108	139	168	182	173	144	109
78	97	127	170	220	265	289	284 278	251 243	203 196	155 148	115	88 85	72 69	63 61	61 59	66 63	79 75	101 95	130 121	157 146	170 158	161 149	134 125	102 95
79 79	98 99	129 131	172 176	222 225	265 266	286 285	274	238	190	143	107	82	67	59	57	61	71	89	113	136	146	139	116	89
80	101	135	180	231	271	287	272	234	186	140	104	80	65	51	55 53	58 56	68 64	84 79	106 99	126 117	136 126	128 119	108 100	83 77
81 82	103	139 144	186 194	238 247	278 287	291 299	274 278	233 234	183 182	137 136	102	78 77	63 62	56 54	52	54	61	75	92	109	117	111	93	72
84	109	149		·25B	299	308	284	236	182	135	99	76	6 L	53	50	52	58	71	87	102 96	109	103 96	87	68 64
86 88	113	156 162	212 221	270 282	311 324	318 330	290 298	239 243	183 184	135 135	99 98	75 74	60 59	52 51	49 48	50 49	56 54	67 64	82 77	90	102 96	91	8 <u>2</u> 77	60
90	121	169	231	294	337	341	305	247	186	135	98	74	59	51	47	47	52	61	73	85	90	86	73	58
91	124	175	240		349 361	351 361	312 319	251 254	187 189	135 135	98 97	73 73	58 58	50 49	46 45	46 45	50 49	59 57	70 67	81 77	86 82	81 78	69 67	55 53
93 95	128 131	181 186	249 257	317 327	371	370	325	257	190	135	97	73	58	49	45	45	48	55	65	75	79	75	64	52
96	134	190	263	335	380	377	330	260	191	135	97	72	57	49	44	44	47	54	64	73 72	77 76	73 73	63 62	51 50
97 98	136 137	194	268 272	342 346	387 390	383 386	333 335	261 261	191 190	135 134	97 96	7≥ 71	57 57	48 48	44 44	44 43	47 47	54 53	63 63	72	76	73	63	50
98	137	197	273	348	392	386	334	260	189	133	95	71	56	48	44	43	47	54	64	73	78	74	63	51
98 98	138 137	197 197	274 272	348 346	39Z 390	385 383	333 330	259 256	188 185	132 131	95 93	71 70	56 56	48 48	44 44	44	47 48	55 56	65 67	75 77	80 82	76 78	65 67	52 54
97	136	195	270	343	385	378	326	252	182	129	92	69	55	48	44	44	49	57	69	80	85	81	70	55
96	134	192	266	338	379	371	319	247	179 174	126	90 89	68 67	55 54	47 47	44 44	45 45	50 51	59 61	71 74	83 86	89 92	84 88	72 75	57 59
95 93	132	189 184	261 254	330 321	371 360	363 352	312 302	24 L 234	169	120	87	66	54	47	45	46	52	63	77	90	97	92	78	62
91	125	178	246	311	34B	340	292	226	164	116	85	65	53	47	45	47	54	65	80	95	102	97	83	65
ลย 85	122	172 165	237 227	299 286	335 320	327 313	281 269	217 208	158 152	113	82 80	63 62	52 52	47 47	45 46	48 49	55 58	68 72	85 90	101	108 116	103	88 94	69 73
83	113	158	216	272	304	2 57	255	198	145	104	77	60	51	47	47	51	61	77	97	116	126	120	101	78
80	108	150	205	257	287	281 263	241	168 177	138 130	100 95	74 71	59 57	50 50	47 47	48 49	53 55	64 68	82 88	105 114	126 137	137 149	13C 141	110 119	84 91
76 73	103 97	142 134	193 181	242 226	270 252	246	226 212	165	122	90	69	56	49	47	50	58	72	95	123	149	161	153	128	98
70	92	126	170	211	235	229	197	155	115	65	66	54	49	48	51	60	77	102	133	161	175	166	139 150	105 113
67 64	87 83	119 112	158 148	197 183	218 203	213 198	184 171	145 135	108	61 77	63 61	53 52	48 48	48 48	52 54	63 66	81 86	109 116	143 154	175 188	190 205	180 194	161	151
61	78	105	138	171	189	184	159	126	96	73	59	51	48	49	55	68	91	124	164	505	220	208	173	129
59 54	74	99 93	130 122	159 149	176 164	171 160	149 139	118	90 85	70 67	57 55	50 49	47 47	50 50	57 58	71 74	95 100	131 139	175 187	216 230	235 251	223 238	184 196	137 146
56 54	71 68	89	115	140	155	151	131	105	81	64	53	48	47	51	60	77	105	147	198	244	266	252	208	154
52	65	85	110	133	147	143 137	125	100 96	78 75	62	52 51	48 47	48 48	52 53	62 63	80 83	110 115	155 162	209 219	258 271	281 295	266 279	219 229	161 169
51 49	63 61	81 79	105 102	128 124	141 136	133	120 116	94	74	59	51	47	48	53	65	85	119	168	228	282	308	290	238	175
48	59	77	99	120	132	129	113	91	72	58	50	47	48	54	66	86	123	174	236	293	319	301	246 253	181 185
47 46	58 57	75 74	97 96	118 116	130	127 125	111	90 89	71 70	58 57	50 50	47 47	49 49	55 55	67 68	90 91	126 129	179 183	244 250	302 309	329 336	310 316	258	189
46	57	73	95	115	127	124	109	88	70	57	50	47	49	56	69	93	131	187	254	314	341	320	261	191
45 45	56 56	73 73	94 94	115	126	124 124	108 109	88 58	70 70	57 57	50 50	47 48	49 50	56 56	70 70	94 94	132 133	188 189	256 256	316 315	343 341	321 320	262 260	191 190
45	56	73	94	115	127	124	109	89	70	57	50	48	50	57	70	94	133	188	254	312	337	315	256	187
45	56	73	95	116	128	126	110	90	71	58	50	48	50	57 57	70 70	94 94	133 132	187 185	251 247	308 301	331 323	309 301	251 244	183 178
45 45	57 57	74 76	97 98	118 121	130	128	112	9 L 9 3	72 73	59 59	51 51	48 48	50 50	57	70	93	130	182	242	293	313	291	236	172
46	59	77	101	124	137	134	118	96	75	60	52	49	50	57	70	93	129	179	236	284	302	279	226	165
47 48	62	80 82	104 108	128 133	142 147	139 144	122 126	98 102	11 19	62 63	53 54	49 50	51 51	57 57	70 70	92 92	127 126	175 172	229 223	274 264	290 278	268 256	216 207	158 151
49	64	86	113	139	154	151	131	106	82	65	55	50	5ì	57	69	91	124	168	217	255	267	244	197	145
51	66	90	118	146	161	157	137	110 114	85 86	67 69	56 57	5 L 5 2	52 52	57 58	70 70	91 91	123 123	166 164	212 207	247 239	256 246	233 222	188 179	138 131
52 54	69 72	94 98	124 130	153 160	169 176	164 172	143 149	118	91	71	59	53	53	58	71	92	123	163	204	232	236	213	170	125
56	75	102	136	167	184	179	155	123	94	73	60	54	54	59	71	92	123	162	201	226	228	204	163	120
58	78	106	141	174	192	187	162	128	98	75	62	55	55	60	72	93	124	162	199	221	221	196	156	115
								1	igu	re A	-4	(She	et 5	of	6)									

Figure A-4 (Sheet 5 of 6)

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Figure A-4 (Sheet 6 of 6)

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141 178 206 216 203 174 138

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ECHELLOGRAM SUBSECTION

TAPE 275 - DESTRUCTIVE R/O SIMULATION(COMPLETE SYSTEM), LAMBDA = 2000 ANGST, SEC PSF WIDTH = 100 MICRONS PTS: 201 TO 225 TOTAL PIXELS = 102400 SUM = 0.1092E 08 RECS: 125 TG 275 AVG = 0.1066E 03232 191 154 125 106 110 133 165 202 237 263 272 AR 112 136 139 174 173 139 112 138 173 212 249 203 166 187 218 117 145 176 1 64 192 210 16B 1.01 1.24 142 155 8B В3 ΒÒ 4B B4 54. >8 B 7 8.7 Q.A 10B 7 C 24C 111 101 ВQ ΒL 154 178 113 102 23L

Figure A-5. Echellogram Subsection - Tape No. 275

115 140 168 194 211 215 206

136 116 103

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150 138

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106 115 119 117 នព 103 111 114 112 100 108 110 108 8.8 7.2 AA. Q.O . 79 9.9 AA QΩ RQ 117 122 112 123 129 QA A3 R7 130 135 142 139 9.2 164 159 170 165 151 132 176 170 181 175 159 162 140 102 122 167 183 187 179 101 120 184 176 180 172 1 32 1 42 5 L 5.8 3.8 3 B SA 3.8 5.7 Figure A-5 (Sheet 2 of 6)

97 116 141 169 194 211 215 205 185 160 135 115 102

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168 193 210 213

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135 151 161 161

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LÚ2 4B A0 RR BO 133 145 143 155 152 165 BO A G 124 14B 170 185 167 134 168 135 1.35 138 166 97 116 194 210 213 142 170 195 211 214 143 170 191 205 145 118 116 140 165 188 201 138 163 184 197 97 115 137 161 182 193 179 190 136 158 177 186 114 135 157 175 183 182

ECHELLOGRAM SUBSECTION

Figure A-5 (Sheet 4 of 6)

	TS: ECS:	226 125		!50 !75			AL PI = 0.			400 S	SUM ≠	0.109	2E 08											
88	98	115	139	167	192	209	213	203	181	155	128	104	85	72	66	65	70	81	95	111	124	129	124	109
86 83	94 90	109 104	131 124	157 147	180 168	195 182	198 185	189 176	169	145	120	98	81	70	65	65	72	84	100	118	132	137	132	116
81	86	99	117	138	158	171	174	165	159 149	136 128	113	93 89	78 75	68 67	64 64	66 67	74 76	87 90	105	124 130	139 146	145 153	139 146	122 128
78	83	94	111	131	149	161	163	155	140	121	102	85	72	65	63	67	77	93	114	135	152	159	152	133
76	80	90	106	124	141	152	154	147	133	115	97	81	70	64	63	67	78	95	117	139	157	163	156	136
73	77	87	101	118	134	144	147	140	127	110	93	79	68	63	62	68	79	97	119	142	160	167	159	139
71 69	74 72	84	97	114	129	139	141	135	122	106	90	77	67	62	62	68	80	98	120	143	161	168	161	140
67	70	81 79	95 92	110	125 122	134 132	137 134	131 128	119 117	103 102	88 87	75 74	66 65	61 61	62 61	68 67	80 80	98 98	120	144	162	169	161	140
65	69	78	91	106	121	130	133	127	116	101	86	74	65	61	91	67	79	97	119	143 142	161 160	168 167	160 159	140 139
63	68	77	90	106	120	130	132	127	116	101	87	74	65	61	61	67	79	97	118	141	158	165	157	137
62	67	77	90	106	121	131	133	128	117	102	87	75	65	61	61	67	78	96	117	139	156	163	155	135
61	66	77	91	107	122	132	135	130	118	103	88	75	66	61	61	67	78	95	116	137	154	160	152	133
60 60	66 67	77 78	92 93	108	124 127	135 138	138 141	132 136	121 123	105	90	77 78	67	62	61	67	78	94	115	136	152	157	150	131
60	67	79	95	113	130	142	145	139	127	108	92 94	80	68 69	62 63	62 62	67 67	77 77	93 93	113	134 131	149 146	154 151	147	128 125
60	68	81	98	117	134	146	150	144	131	114	97	82	71	64	63	67	77	92	110	129	143	147	139	121
61	69	63	101	121	139	152	156	150	136	119	100	85	73	66	64	67	77	91	108	126	139	143	135	118
62	71	86	105	126	145	159	163	157	142	124	105	88	75	67	65	68	76	90	106	123	135	138	130	113
63 65	74 77	90 94	110 116	132	153	167	171	165	150	130	011	92	78	69	66	68	76	89	104	120	131	133	125	109
67	80	99	123	149	162	177 189	182 194	175 187	159 169	138 146	116 123	96 101	81 85	71 74	67 69	69 70	76 76	88 87	102 101	117 114	127 123	129	121	105
70	85	105	131	159	185	203	208	200	181	157	131	108	89	77	71	71	77	87	99	112	120	124 120	116 112	101 98
73	89	112	140	171	199	218	224	216	195	168	140	114	94	81	73	73	77	87	98	110	117	117	109	94
77	95	120	151	184	215	236	242	233	210	181	150	122	100	85	76	74	78	97	98	109	115	114	106	92
81	101	128	162	199	232	255	262	252	227	195	161	131	106	89	79	77	80	88	98	108	114	112	104	90
85 90	107 114	137 147	174 187	215 232	251 272	277 299	284 307	273 295	246 265	210 226	173 186	139 149	113 120	94 99	83	79	82	89	99	108	113	111	102	88
95	121	157	201	249	293	322	331	317	285	242	198	158	127	104	87 91	82 86	84 87	91 94	101	109 112	114	111	102 102	87 87
100	128	167	215	267	314	346	355	339	304	259	211	168	134	109	95	89	91	98	107	115	118	114	104	88
105	135	177	228	264	334	369	378	361	323	274	223	177	140	115	99	93	95	102	111	119	122	118	106	90
109	142	187	241	301	354	39¢	400	382	341	289	234	186	147	120	104	97	99	107	117	125	127	122	110	93
114 118	148 154	196 204	253 264	316 330	372 389	410 428	420 438	401 417	358 372	302	245	194	153	125	109	102	104	112	123	131	133	127	114	96
122	159	211	274	342	403	443	453	431	384	314 323	254 261	201 206	158 163	129 133	112	106 111	109 114	118 124	129 136	138 146	140 148	133	119 124	99 103
125	164	217	281	35 L	413	455	465	441	392	330	267	210	167	136	120	115	120	131	144	154	156	147	130	107
128	167	221	287	358	421	463	472	448	398	334	270	213	169	139	123	119	125	138	152	162	164	155	136	112
130	170	224	290	362	425	466	475	451	400	336	271	214	170	141	125	123	130	144	159	170	172	162	142	116
131	171	225 225	291 290	362	425	466	474	449	398	334	270	214	170	142	128	126	135	150	167	179	180	169	147	120
132 132	171 170	223	287	360 356	422 416	462 454	469 461	444 435	393 385	330 323	266 261	211 208	169 167	142 141	129 130	129 132	140 144	156	174	186	198	176	153	124
132	169	220	282	348	406	443	448	423	374	313	254	203	164	140	130	133	147	162 167	101 187	194 201	195 202	182 188	158 163	128 131
131	166	216	276	339	395	429	433	408	360	302	245	197	160	138	130	135	150	171	193	207	208	193	167	134
129	163	211	268	329	381	413	416	391	345	290	236	190	156	136	129	136	152	175	197	212	212	198	170	137
127	160	205	260	317	366	395	398	373	329	277	225	182	151	133	128	136	154	177	200	215	216	200	172	138
126 123	156 153	199 193	251 242	304 292	350 334	377 359	379 359	355 336	313 296	263 249	215 204	174 166	145 140	129	126	135	154	178	202	217	217	202	173	138
121	149	187	233	280	319	341	340	317	279	235	193	158	134	125 121	123 120	133 131	153 151	178 175	201 199	216 213	217 214	201 197	172 169	137
119	145	181	224	268	303	323	321	299	263	222	182	150	128	116	116	127	147	171	194	208	20B	192	164	135 131
117	142	176	216	257	289	306	304	282	248	209	172	142	121	iii	112	123	142	166	187	201	201	185	158	126
115	139	171	209	246	276	291	288	267	234	197	162	135	116	106	108	118	136	159	179	192	191	176	151	120

TAPE 275 - DESTRUCTIVE R/D SIMULATION(COMPLETE SYSTEM), LAMBDA = 2000 ANGST. SEC PSF WIDTH = 100 MICRONS

R-26

112 111	136 134 132	167 164 161	203 198 194	236 231 225	265 255 247	278 266 256	273 260 249	240 229	209 199	176 168	154 146 138	128 121 115	110 105 100	97 92	103 98 93	107 102	130 123 116	143 134	170 161 151	182 171 161	181 170 160	167 157 147	143 134 126	114 108 102
110	131	159	191	220 217	241	248	240 233	219	191	160 154	132	110 105	95 91	88 84	8 8 8 4	96 91	110 103	126 118	141 132	150 140	149 139	138 128	118 110	96 9 0
110	131	159 160	188	215 215	233	237 235	227 224	206 202	173	148	122	101 98	87 84	80 77	80 77	86 82	97 92	111 104	123 115	131	130 121	120 112	103 96	84 79
111 112	134 136	162 165	192 195	217 221	233 235	234 236	222 223	199 199	171 170	142 140	116 114	96 94	82 80	74 72	73 70	78 74	86 82	98 92	108 101	113 106	112 105	104 97	90 84	74 69
114 117	139 143	170 175	201 207	226 233	240 247	240 245	225 229	200 202	170 171	140 140	113 113	92 92	78 77	70 68	68 65	70 67	77 73	86 81	94 88	99 92	98 91	90 84	78 73	65 61
120 123	148 153	182 188	215 223	241 250	255 263	252 259	234 239	206 209	173 175	141 142	113 113	91 91	76 75	67 66	63 62	65 62	- 70 - 67	77 73	83 79	87 82	68 18	79 75	69 65	58 55
127 130	158 164	195 202	231 239	259 268	271 280	266 273	245 251	213	177 180	143	113	90 90	74 74	64	60 59	60 58	64 62	69	75 71	77 74	76	71	62	52
133 136	168	209	247 254	276 283	288 295	280	256	221	182	145	114	90	73	63	58	57	60	64	68	71	72 69	67 65	59 57	50 48
139	1.77	220	260	290	301	286 291	260 264	224 226	184 186	146 147	115	90 90	73 73	62 62	57 56	56 55	58 57	62 61	66 64	68 66	67 65	62 61	55 54	47 46
141 143	189 182	224 22 7	265 269	295 298	376 309	295 298	267 269	228 229	186 187	148 147	115 115	90 90	72 72	61 61	56 55	54 54	56 56	60 59	63 63	65 65	64 64	60 60	53 53	45 45
144 144	184 184	229 229	270 271	300 300	310 310	298 298	269 268	229 227	186 185	147 146	114	89 89	72 71	61 61	55 55	54 54	56 56	60 60	63 64	66 67	65 66	61 62	54 55	46 46
143 143	184 182	228 227	270 268	299 296	308 305	296 292	265 262	225 222	183 180	144 142	112	88 87	71 70	60	55 55	54 55	57 58	61 63	66 67	68 70	68 70	63	56	47
141	181 178	224	264 259	292 286	300 294	20B 281	258	219	177	146	109	86	70	60	56	56	59	65	70	73	72	65 68	58 60	49 50
137	174	215	253	219	287	274	252 245	214 208	173 169	137 133	107 104	84 83	69 68	60 60	56 57	57 58	61 62	66 69	72 75	76 79	75 78	70 73	62 64	52 54
133	169 164	20.3 20.3	246 237	271 261	278 268	265 256	237 229	201 194	163 158	129 125	102 99	81 79	67 6 6	60 60	57 58	59 61	64 67	71 75	78 82	82 87	82 87	77 81	68 71	57 60
125 121	158 152	195 186	228 218	251 239	257 245	245 234	219 209	186 178	152 145	121 116	96 93	77 76	66 65	60	59 60	62 65	70 73	79 83	87 93	93 99	93	87 93	76 81	63
116	145	177	207	227	232 219	222	198 187	169	138	111	89	74	64	60	62	68	77	89	100	107	107	100	88	67 72
106	131	159	184	201	206	196	176	150	131 124	106	86 82	72 70	63 63	61 61	63 65	71 75	82 88	95 103	108 116	115 125	116 125	108 117	94 102	77 83
101 96	124 117	149 140	173 162	188 176	192 179	183 171	164 154	141 132	117 110	95 91	79 76	68 66	62 62	62 63	68 70	78 83	93 99	110 118	125 135	135 145	136 146	126 136	109 118	89 95
91 86	110 103	131 123	151 141	1 54 1 53	167 156	165 149	144 135	124 116	104 98	86 82	73 70	65 64	62 62	65 66	73 76	87 91	106	126 135	145 155	156 168	157 169	146 157	126 135	102 109
51 77	98 92	l 16 109	132 124	143 134	146 137	140 131	126 119	109	93 88	78 75	68 66	62 62	62 62	67 69	79 82	96 101	119	143 152	165 176	179 191	180 192	168 178	144	116
74 71	87 83	103 98	117	127 120	129	123	112	98	84	72	64	61	63	70	85	106	132	161	1 86	202	204	189	162	129
6.8	80 77	94	106	115	117	112	102	90	81 78	7 C 6 9	63	6 L	63 64	72 74	88 91	110	139 145	169 178	197 206	214 224	215 226	199 209	170 178	136 142
66 64	75	90 88	102 99	111 107	113	108	99 97	88 86	76 75	67 66	62 61	61 61	65 66	76 77	94 96	119 123	151 156	185 192	215 224	234 243	235 244	218 225	185 192	147 152
61	73 72	85 84	97 95	105 103	107 105	103 162	95 94	84 83	74 73	66 66	61 61	62 61	67 67	79 80	99 101	127 130	161 165	198 203	231 237	251 257	252 258	232 237	197 201	156 159
60 59	71 70	83 62	94 93	192 191	104 104	101	93 93	83 83	73 73	65 65	61 61	62 62	6B 69	81 82	102 104	132 134	168 17G	207 209	241 243	261 264	262 264	241 242	204 205	161 162
59 58	70 69	82 82	93 93	101 102	104 104	100	93 93	83 83	73 73	66 66	62 62	63 63	69 69	83 83	104 105	134 134	171 171	210	244	264 262	264 261	242	204	161
5 a 59	70 70	82 83	94 95	102	105	102	94 95	84 85	74 75	66 67	62	63 63	70 70	83	104	134	170	208	240	259	257	240 236	199	159 156
59 60	71	84	97	106	109	105	97	87	76	68	63 64	64	70	83 83	104 103	133 131	168 165	205 201	236 231	254 247	252 245	230 224	194 189	153 148
61	7 <u>2</u> 74	86 89	105	108	ill 115	108 111	99 102	89 91	78 80	69 71	65	64 65	70 70	82 82	102 101	129 127	162 159	196 191	225 218	240 232	237 229	216 208	182 175	143 138
63 65	76 79	92 95	106 110	115 120	119 123	115 120	106 110	94 97	82 85	72 74	66 68	65 66	70 70	81 81	100 ·	125 123	155 152	186 181	211 204	224 216	220 212	200 192	168 161	133 127
67 69	88 86	99 103	114 119	125 131	129	125 130	114 119	101 105	87 90	76 78	69 71	67 68	71 71	81 81	98 98	121	149	176 172	198	208	204 196	184	155 148	122
7 <u>2</u> 75	89 93	108	125 130	137 143	140	135	124	109 113	93 97	81 83	72 74	69 71	72 73	81	97	119	144	169	187	195	189	170	142	113
78	97 100	117	136	149	153	147	134	117	100	86	76	72	74	82 83	97 98	118 118	143 142	166 163	183 179	189 185	183 177	164 158	137 132	10B 105
83 84	194	127	142	155 162	159 166	153 160	140 146	122 127	104 108	89 92	78 81	74 76	76 77	84 85	100 99	1 19 1 19	141 141	162 161	176 175	181 178	173 169	154 150	128 125	101 99
87	109	133	155	169	174	167	152		112	95 •o. A.	63 _5	78 (Cho	79 et 5	87 . a.e.	101	121	142	162	174	176	167	147	122	97
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162 177 182 175

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Figure A-5 (Sheet 6 of 6)

ECHELLOGRAM SUBSECTION

TAPE R13 - NON-DESTRUCTIVE R/O SIMULATION(COMPLETE SYSTEM), LAMBDA = 2000 ANGST, SEC PSF WIDTH = 50 MICRONS

	PTS: RECS:	201 125		225 275				XELS 1089E		400 SI	JM = (0.111	5E 08											
35 37	3 430	397	305	210	137 141	96 99	74 76	62 64	57 59	57 59	62 64	74 77	97 103	141 149	20 7 221	279 299	316 338	294 313	231 243	164 171	114	85 87	68 69	61 61
39			316	216	144	101	77	65	60	60	66	80	107	158	235	318	360	331	255	178	122	88	70	61
41 42	-		325 330	220 222	146 147	102 103	78 78	66 66	61 61	61 62	68 69	83 85	112 116	166 173	248 260	337 354	381 400	349 366	267 279	184 191	125 128	90 92	71 72	62 62
42			330	222	147	102	78	66	62	63	70	87	119	179	270	368	416	380	288	196	131	93	72	61
41					145	101	78	66	62	63	71	88	121	183	277	379	428	390	295	200	133	94	72	61
41			319	214	142	100	77	66	61	63	71	8.8	122	185	281	384	434	395	298	201	133	94	72	61
39: 37:			308 294	207 199	138 132	97 94	75 73	65 63	61 60	63 62	71 70	88 87	122 121	185 183	281 277	384 379	434 428	395 388	297 292	200 197	132 130	93 91	71 70	60 59
35				189	127	90	71	62	58	61	68	85	118	178	271	369	416	378	284	191	127	89	69	58
3 3				178	120	87	69	60	57	59	67	83	115	173	261	355	400	364	274	184	123	87	67	56
31				167	113	82	66	58	55	57	65	80	111	165	249	339	381	346	261	177	118	84	65	55
29 26:			227 20B	155 143	106	78 73	63 60	56 53	53 51	55 53	63 60	77 74	106	157 148	235 220	319 297	359 334	326 304	247 230	167 157	113 107	81 77	63 61	54 52
24			190	132	92	69	57	51	49	51	58	70	94	138	204	274	308	280	213	147	100	73	58	50
22				121	85	65	54	49	47	49	55	67	89	129	189	252	282	257	197	136	94	70	56	49
19			157	111	79	61	51	46	45	47	52	63	83	120	174	232	259	236	181	126	8.8	66	54	48
17 16				101 91	73 67	57 53	4B 46	44 42	43 41	45 43	50 48	60 57	79 74	111	161 150	213 198	23B 220	218 201	167 156	118 110	83 79	63 60	52 50	46 45
14			115	83	62	50	43	40	40	41	46	54	70	98	140	184	205	187	145	103	74	58	49	44
13		-	105	77	58	47	41	39	38	40	44	52	66	92	131	172	191	175	135	96	70	55	47	44
12			9 7	71	54	44	39	37	37	38	42	50	63	87	124	162	179	163	126	91	67	53	46	43
11			91	67	51	42	38	36	36	37	41	48	6 L	83	117	153	169	154	119	86	64	51	45	43
11. 10			86 82	64 61	49 47	41 40	37 36	35 34	35 34	36 35	40 39	46 45	58 56	80 77	112	146 140	161 154	147 141	114 109	82 73	61 60	50 49	45 44	43 43
10.			80	60	46	39	35	33	33	34	38	44	55	74	104	135	149	136	106	77	58	49	44	43
10	101	99	78	58	45	38	34	33	33	34	37	43	53	72	101	131	144	132	103	75	57	48	44	43
9			77	58	45	37	34	32	32	33	36	42	52	70	98	127	140	128	100	74	57	48	44	44
9.			77 77	57 57	44 44	37 37	34 33	3 <i>2</i> 32	32 32	33 33	36 36	41 41	51 50	69 68	95 93	123 120	136 133	124 121	98 96	72 71	56 56	48 48	45 45	45 45
9.			77	57	44	37	34	32	32	33	35	40	50	67	92	118	130	119	94	71	56	48	46	46
9		_	77	58	45	37	34	32	35	33	35	40	50	66	90	116	128	117	93	70	56	49	46	48
10 10			78 80	58 60	45 46	3B	34 34	3 <i>2</i> 33	32	33	35	40	50	66	90	116	127	117	93	70	56	49	47	49
10			82	6 L	47	36 39	35	33	32 33	33 34	36 36	4 <u>1</u> 41	50 50	66 67	91 92	116 118	128 130	110 119	94 95	71 72	5 <i>1</i> 58	50 51	48 49	50 51
11			86	63	49	40	36	34	33	34	37	42	51	68	93	120	132	122	97	73	59	52	50	53
11.			90	66	51	42	37	35	34	35	37	43	52	70	96	123	136	124	99	75	60	53	52	54
12 13			95 102	70 74	53 56	43 45	38 39	36 37	35 36	36 37	38 39	44 45	54 55	71 74	98 102	126 131	139 145	128 133	102 105	77 79	61 63	54 56	53 54	55 57
14			110	80	59	47	41	38	37	38	40	46	57	75	106	137	151	138	109	82	65	57	55	58
15			120	86	63	50	43	39	38	39	42	48	59	80	111	143	158	145	114	85	67	59	57	59
17			131	93	67	53	45	41	39	40	43	50	62	84	116	151	166	152	119	89	69	60	5.8	60
19. 21			144	100	72 77	56 59	47 49	43 44	41 42	42 43	45 46	52 54	65 68	88 94	123	160 171	176 188	161 171	126 133	93 97	72 75	62 64	59	61
23.			171	117	82	62	52	46	44	45	48	57	72	100	141	183	201	183	141	102	77	65	60 61	62 63
25				126	87	66	54	48	46	46	50	59	77	107	151	196	216	195	150	107	81	67	62	63
27			200	135	93	69	56	50	47	48	52	62	81	113	161	210	230	208	159	113	84	69	6.3	64
29			215 229	144 153	98 103	72 75	58 61	51 53	49 50	49 51	54 56	65	85	120	171	223	245	221	168	118	87	71	64	64
3 Li 3 3 :			241	160	107	78	62	55	51	52	58	67 69	88 92	126 131	180 190	236 249	260 274	234 246	. 177 185	124 129	90 93	72 74	65 66	65 65
350				167	111	80	64	56	53	54	59	71	_	137	198	260	287	257	193	134	95	75	67	65

Figure A-6. Echellogram Subsection - Tape No. 813

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363	399	354	260	172	114	82	65	57	54		60	73			206 213	271 280		267 275	200 205	137 141	97 99	76 77	67 67	65 65
372	409	363	266	176 178	116 118	84 85	66 67	58 58	54 55		62 63	77	104	150	218	287	315	281	210 212	143 145	100	76 78	68 67	65 64
377 378		367 368	269 270	178	118	85	67	59	55 55	57 57	63 63				222 223	291 293	319 321	285 286	213	145	101	78	67	64 64
376	412 405	365 358	268 263	177 174	117	85 84	67 67	59 58	55	57	63	78	106		222 220	291 287	319 314	284 280	212 209	144 142	101 99	78 77	67 66	63
370 362	394	348	256	170	114	82	66 6 5	58 57	55 54	56 56	63 63		105 104	152 150	216	281	307	273	204	139	98 96	76 75	66 65	63 62
351 338	381 365	336 322	248 237	165 159	111	81 79	64	56	54	55	62	76 75	103 101	148 145	211 206	273 265	298 287	265 255	198 191	136 132	93	73	64	62
323	347	306	226	152	103	76 74	62 61	55 54	53 52	55 54	61 61		100	142	200	256	276	245 233	183 175	127 122	91 88	72 70	63 62	61 61
307 291	329 310	289 272	214 202	145 137	95	71	59	53	51	53 52	60 59	73 72	99 97	139 136	194 188	246 235	264 250	221	166	117	85	68	61	60 60
275	291	254 238	189 177	129 122	90 86	69 66	57 55	52 50	50 49	51	57	71	95	132	180	223 211	236 222	208 195	157 148	111	82 78	66 65	60 59	60
260 246	272 255	222	165	115	82	63	54	49 48	48 47	50 49	56 55	69 68	92 90	128 124	172 165	500	208	183	139	100	75	63 61	58 58	59 59
234 224	240 226	20 <i>1</i> 194	155 145	108 102	78 74	61 59	52 51	47	46	48	54	67	89 88	121 118	159 153	189 179	195 182	170 158	130 121	94 89	72 69	60	57	59
215	214	182	136	97	71 68	57 55	49 48	46 45	45 44	47 47	54 53	66 65	86	116	147	169	170	147	113 105	84 80	66 64	58 57	56 56	59 59
208 202	203 195	172 163	129 122	92 88	66	54	47	44	44	46 46	52 52	65 64	85 84	113	142 137	160 152	159 148	136 127	99	75	62	56	55	59
198	198 184	156 151	117	85 82	64 63	52 51	46 46	43 43	43 43	45	52	64	84	110	133	145 140	139 132	119 112	93 88	72 69	60 58	55 54	55 54	59 59
197 199	182	148	110	80	61	5 L	45 45	4.3 4.3	43 43	45 45	51 52	64 64	84 84	109 109	130 130	137	127	107	84	66	57	53 52	54 54	59 59
203 209	1.83 1.85	146	109	77 79	61 61	51 51	45	43	43	46	53	45	86 89	111 115	131 134	136 137	125 124	104 102	81 80	65 64	56 55	52	54	59
219	189	147	108	79	61 61	51 51	46 46	43 44	43 44	46 41	54 55	67 69	93	120	139	140	124	101	78 78	63 62	54 54	52 51	53 53	59 59
228 242	195 203	149 153	109	79 80	62	52	47	44	45	48	56 58	72 75	97 102	125 132	144 151	144 149	125 128	100 100	77	62	54	51	53	58
259	213	159	113	82 84	64 65	53 54	47 48	45 46	46 47	50 51	61	79	108	140	160	155	131	101	77 78	62 62	53 53	51 51	52 52	58 57
278 300	226 241	166 174	122	87	67	55	5 C	47 48	48 49	53 54	63 66	83 86	114	149 159	169 180	162 171	135 140	106	79	62	54	50	52 51	57 56
323 347	256 272	183 191	126 131	90 93	69 71	57 58	51 52	49	51	56	69	92	129	170	192 204	181 191	146 153	109	80 82	63 63	54 54	50 50	51	55
371	288	200	136	95	72	60 61	53 54	51 52	52 53	58 60	72 75	97 103	138 146	181 193	217	202	160	115	83	64	54 54	50 50	50 50	54 53
395 418	304 319	209 218	140 145	98 101	74 76	62	55	53	55	62	77	108 112	154 162	205 215	230 242	213	167 174	119 123	85 87	65 66	55	50	49	52
439	333	226		103 105	78 79	63 64	56 57	54 55	56 57	63 65	80 83	116	169	225	253	232	180	126 130	89 90	66 67	55 55	49 49	48 47	51 50
455 466	344 352	232 236	155	106	80	65	57	55 55	57 58	66 67	85 86	120	175 180	233 241	262 271		185 190	132	91	67	55	49	47 46	48 41
472 471	355 354	23B 237			80 80	65 65	58 58	56	58	68	87	125	184	247 250	277 280		193 194	133 133	91 91	67 67	54 54	48 47	45	46
466	350	234	153	106	79 78	65 64	58 57	56 55	58 58	68 68	88 88	126	186 187	251	28 L	255	193	132	90	66	53 52	47 46	44 43	45 44
457 444					77	63	56	55	58	67	87	126 123	185 182	248 243	278 272		190 186	130 127	89 87	65 64	51	45	42	42
429	322	217			75 73	62 61	56 54	54 53	57 56	66 65	86 84	120	176	236	264	240	181	124 120	85 82	62 61	50 49	44 43	41 40	41 40
411 391			132	92	71	59	53	52	54 53	63 61	82 19	116	170 163		254 243		175 168	115	80	59	48	42	39	39 38
370 348						57 55	52 50	50 49	51	59	76	107	155	207	Z31 219			111		57 55	46 45	41 40	38 37	37
326	246	167	112	80	_	53 51	48 47	47 45	50 48	57 55	73 69	102 97	148 139		206	188	144	100	70		43 42	39 37	37 36	37 36
304 282			_			49	45	44	46	52	66 63	9 Z 86	131 122					95 88		-	40	36	35	35
262	199	136				47 45	43 41	42 41	44 42	50 48	59	80	113	148	164	149						35 34	34 33	35 34
242 225			9 8	3 61	50	43	40	39	41 39	45 43	56 52	75 70						69	51	41	36	33	33	34 34
208						41 40	38 37	37 36	37	41	49	65	88	113	124							33 32	32 32	33
194		9	7 6	9 5	4 3	38	36 24	35 34	36 35	39 38	47 44	60 56				3 94	75	56	, 43	36	33	31 31	32 31	33 33
17:						37 36	34 33	33	33	36	42	53	70	88								31 31	31	33
159) L2i	L 8	5 6	1 4	7 39	35 34	33 32	32 31	32 32	35 34	40 39	51 49		79	86	5 79	6.3	49	34	3 34	31	31 31	31 32	34 34
151 149				8 4	5 38	34	31	31	31	33	38	47	61							3 33	31	31	32	35
1.49	5 111	L 7	8 5			33 33	31 31		31 30	33 32	37 37	46 46	, 5°	74	4 ₿(0 74	§ 59	9 40	5 3			31 31	32 33	35 36
14. 13:				5 4		32			30	32		46					יכיי	, 40	, ,	, -		- -		
									Fi	gure	A-6	•	(She	et 2	2 of	6)								

45 37 4 L 59 46 116 127 45 57 149 Вì 52 65 51 159 175 L46 61 53 53 54 54 55 55 4 B 232 255 227 248 272 242 262 287 256 145 210 275 301 267 311 276 77 103 53 53 56 154 222 293 319 225 292 317 281 26 L 313 277 157 224 306 270 219 277 298 81 110 82 110 156 216 271 289 254 247 219 149

ECHELLOGRAM SUBSECTION

TAPE 813 - NON-DESTRUCTIVE RID SIMULATION(COMPLETE SYSTEM), LAMBDA = 2000 ANGST, SEC PSF WIDTH = 50 MICRONS

	: 23 : 23	226 1 125 1		50 75				XELS 1089E		400 S	UM =	0.111	5E 08											
59	63	72	91	126	190	288	391	440	399	30C	201	133	93	70	57	50	47	47	52	63	83	114	144 155	155 166
59	62	70	88	121	180	270	366	411	373	281	190	126	89	68	56	49	47	48 49	53 55	66 69	89 95	122 131	166	178
59	61	68	84	115	169	252	340	382	347	262	178	119	85	65 63	55 53	49 48	47 47	50	57	73	101	141	179	191
58	60	66	81	109	159	235	316	354	321	243	166 155	112 106	81 77	61	52	48	47	51	59	76	107	151	193	206
58	59	64	78	103 98	149	219 204	293 272	328 304	298 276	226 210	145	100	73	59	51	47	48	52	δí	80	113	161	207	222
57	57	62	74 71	93	140 131	191	253	282	256	196	136	94	76	57	50	47	48	52	63	84	120	172	221	237
56 55	56 55	61 59	6.8	88	124	178	236	262	239	182	127	89	67	55	49	47	48	53	65	88	127	102	235	252
55	54	57	66	84	117	167	220	245	222	170	119	84	64	53	48	46	48	54	67	91	132	191	247	264
53	52	55	64	80	111	158	207	229	208	160	112	80	62	52	47	46	48	55	68	93	137	198	256	275
52	รัเ	54	61	77	106	150	195	216	196	150	106	76	59	51	46	46	48	55	69	95	1.40	203	263	281
51	50	53	60	74	102	143	187	206	187	143	101	73	58	49	46	45	48	55	70	96	142	206	266	285
50	49	51	58	72	98	138	180	198	180	138	98	71	56	49	45	45	48	56	70	97	143	207	267	Z86
49	48	50	57	71	96	135	175	193	175	134	95	70	55	48	45	45	48	56	70	97	143	206	267	286
48	47	49	56	70	95	133	173	191	173	132	94	69	55	48	45	45	48	56	70	97	142	205	264	283
47	46	49	56	69	94	132	172	190	172	132	94	68	54	47	44	45	48	55	70	96	141	203	261	279 275
46	46	48	55	69	94	133	173	191	173	132	94	68	54	47	44	45	48	55	69 69	95 95	139 138	200 197	257 253	270
45	45	48	55	69	95	134	175	193	175	134	95	69	55 55	47 48	44 45	45 45	48 48	55 55	69	94	136	194	248	264
44	45	48	55	70	96	136	178	196 201	178 182	136 139	96 98	70 71	56	48	45	45	48	55	69	94	135	192	244	259
43	44	48 48	56 56	7 L 72	98 100	139 142	182 197	207	187	142	100	72	57	49	45	45	48	55	69	94	135	189	239	252
43 43	44 44	49	57	74	103	147	193	213	192	147	103	74	58	50	46	45	48	55	69	93	133	186	232	244
43	45	49	59	76	106	152	199	220	199	151	106	76	59	50	46	46	48	55	68	93	131	181	225	235
43	45	50	6ว์	78	119	158	207	229	207	157	110	78	61	52	47	46	49	55	68	92	129	176	217	225
43	46	52	63	82	116	166	218	241	217	165	115	81	63	53	46	47	49	55	68	19	126	171	208	214
43	47	53	65	86	123	176	231	254	229	173	120	85	65	55	49	48	49	55	68	90	124	165	199	204
44	48	55	68	91	131	188	246	271	243	184	127	89	68	56	51	48	50	56	68	90	122	161	190	193
45	49	58	72	97	140	202	264	291	261	196	135	94	71	58	52	50	51	56	68	90	121	157	183	183
46	51	60	76	104	150	218	285	313	281	21C	144	100	75	61	54	51	52	57	69	90	120	154	176	175
47	53	63	81	111	162	235	309	340	303	227	154	106	78	64	56	52	53	58	70	91 92	120 120	151 149	171 166	167 161
49	55	66	85	119	175	256	336	369	329	245	166	113	83	66 70	58 60	54 55	54 55	59 60	71 72	93	122	149	163	155
50	57	70	91	128	189	278	366 398	402 438	358 390	266 288	178 192	120 129	68 93	73	62	57	57	62	74	96	124	149	160	150
52	60	73 77	96	137 146	205 220	301 326	433	476	423	312	207	137	98	76	65	59	59	64	77	99	128	152	160	147
53 55	62 65	81	102 108	156	237	352	468	515	457	336	221	146	103	80	67	6i	61	66	80	103	133	156	161	146
57	67	84	114	166	253	377	502	553	491	360	236	154	109	84	70	64	63	69	83	109	140	163	165	147
59	70	88	119	175	268	402	535	590	523	382	250	163	114	87	73	66	65	71	88	115	148	171	171	149
60	72	91	125	103	283	424	567	625	553	404	263	170	118	90	75	48	68	75	92	122	157	181	178	153
62	74	44	130	191	296	445	595	656	580	423	275	177	123	93	78	70	70	78	97	130	168	192	187	158
64	76	97	134	198	307	463	620	683	604	440	285	183	127	96	80	72	73	81	103	139	179	204	197	164
65	78	100	137	204	317	478	640	705	623	453	293	188	130	96	82	75	75	85	109	148	192	218	208	170
66	79	102	140	209	325	490	655	721	637	463	299	192	132	100	84	76	78	89	115	158	206	232	219	177
67	8.0	10.3	143	212	329	497	663	730	645	468	303	194	134	102	85	78	80	92	121	168	219	246	231	185
68	81	104	144	214	332	499	665	732	646	469	303	195	134	102	86	79	82	96	127	177	232	261 274	242 254	192 198
69	82	104	144	214	331	497	66 L	726	641	465	301	194	134	103	86	80	84	99	133	186	245 257	288	264	205
69	82	104	144	213	329	491	651	714	630	458	297	191	133 131	102 101	87 86	81 82	85 87	102 105	138 143	195 204	269	300	274	211
70	82	104	143	211	324	482	636	696 672	613 591	446 430	290 281	188 183	128	100	86	82	88	107	148	212	280	312	284	217
70	32	103	142	209 205	318 311	470 455	61 <i>7</i> 593	644	266	412	270	177	125	98	85	82	88	109	151	219	290	323	293	222
70 70	81 81	102 101	140 138	201	302	439	568	613	538	392	258	170	121	96	84	81	89	110	154	224	298	332	300	226
69	80	100	135	197	293	422	541	580	508	371	245	163	117	93	82	80	88	111	156	228	304	338	305	229
69	79	98	133	192	285	405	514	548	478	350	232	155	112	90	80	79	88	ili	157	229	306	340	306	229
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Figure A-6. (Sheet 4 of 6)

68	78	97			_		486			328		147	108	87	76	78	86	109	155	228 223	304 298	338 331	304 297	227 222
68	77	95	128	184	268	37l	460	482 451	418 389	306 286	205 192	140 132	103 98	84 81	76 73	76 74	85 82	107 104	153 148	216	289	320	287	214
67 67	76 76	94 93	126 125	180 177	260 253	355 341	434 411	422	362	266	180	125	94	78	71	71	80	101	143	208	276	306	274	205
66	75	92	123	175	249	330	390	395	337	248	169	118	89	75	68	69	77	97	L 36	197	261	289	259	194
66	74	91	123	174	245	321	372	372	315	231	158	111	85	72	66	66	74	93	129 122	186 174	245 229	271 253	243 227	182 171
65	74	91	123	174	243	313	357	351	294 276	216 202	149 140	105 100	81 78	69 66	63 61	64 61	71 68	88 84	115	163	213	235	211	159
65 65	74 73	91 91	123 124	175 176	242 243	308 304	344 333	332 317	260	190	132	95	74	63	59	59	65	79	108	152	198	218	197	149
65 64	73	92	125	178	245	302	326	304	247	180	126	91	71	61	57	56	62	75	101	142	184	203	183	139
64	74	93	127	182	249	303	321	294	236	171	120	87	69	59	55	54	59	71	95	132	171 159	188 174	169 156	129 119
64	74	94	130	187	254	307	319	287	228 221	164 159	115 112	84 82	67 65	57 56	53 51	52 51	57 54	67 64	89 84	123 115	147	161	144	110
64 65	75 76	96 98	134 138	193 201	262 273	313 323	3 <i>2</i> 0 325	283 282	217	155	109	80	63	54	50	49	52	61	79	107	136	149	133	102
65	78	101	144	210	285	336	333	284	216	152	107	78	62	53	49	48	50	58	74	100	127	138	124	95
66	79	104	150	221	300	351	344	288	215	151	105	77	61	52	48	46	48	55	70	94	118	128	115	89
66	81	108	157	232	316	367	355	293	215	150	104	76	61	52 51	- 47 46	45 44	47 45	53 51	67 63	88 83	110 104	119	107	63 78
67	82	111 115	164	243 255	332 348	384 400	367 379	298 304	216 217	149 148	103	76 75	60 60	50	45	43	44	49	61	79	98	105	95	74
68 68	84 86	119	177	266	363	416	391	309	218	148	102	75	59	50	45	43	43	48	58	75	93	100	90	70
69	88	122	183	276	377	430	402	314	219	147	102	75	59	50	44	42	42	47	56	72	89	95	86	67
70	89	124	188	285	389	444	411	319	221	147	101	74	59	49	44	41	42	46	55	70	86	92 90	83 81	65 64
70	90	127	192	292	400	455	420	323	221	147	101 100	74 74	58 58	49 49	44 43	41 41	41 41	45 45	54 53	68 68	84 83	89	80	63
79 71	91 92	128 130	196 198	298 302	408 412	463 468	425 428	325 326	222 221	146 146	100	73	58	49	43	4 L	41	45	54	68	83	89	81	64
71	92	130	199	303	414		429	325	219	144	99	73	58	49	43	41	41	45	54	69	85	91	82	65
71	92	130	199	303	414		427	323	217	143	98	, 72	57	48	43	41	41	45	55	71	87	94	85	66
70	91	159	198	302	412	466	424	320	215	141	97	71	57	48	43	4 L	42	46	56 58	73 75	90 94	97 101	88 91	68 71
7 ^	90	128	196	299	408	461	419	315 309	211 207	139	95 94	71 70	56 56	48 47	43 43	41 41	42 42	47 48	59	78	97	105	95	73
69 68	89 88	126 124	193 189	294 288	402 393	453 442	411 401	301	202	133	92	68	55	47	43	41	43	49	61	91	101	110	99	76
67	86	121	184	280	381	429	389	292	196	129	89	67	54	47	43	42	44	50	63	84	106	115	103	80
66	84	118	176	270	368	414	376	282	190	125	87	66	53	46	43	42	45	52	66	89	112	121	109	84
64	82	114	172	260	353	398	361	272	183	121	85	64	53	46	43	43	46 47	54 56	70 74	94 100	119 128	129 139	116 125	89 95
63	79	106	165 158	249 237	338 321	380 361	345 328	260 248	176 168	117	82 80	63 61	52 51	46 46	43 43	43 44	49	59	79	108	139	151	135	103
61 59	77 74	101	150	224	302		309	234	159	107	77	59	50	45	44	45	51	63	85	118	152	165	147	111
58	71	96	142	210	283	318	289	219	150	102	73	58	49	45	44	46	53	67	92	128	165	1.80	160	120
56	68	91	133	197	264	296	269	204	140	96	70	56	48	45	45	48	55	71	99	139	180	196	174	130
54	65	87	125	184	246	275	250	190	132	91 86	67 64	54 53	48 47	45 45	45 46	49 50	58 61	76 80	106 114	151 163	196 212	213 231	189 205	140 152
52 50	62 60	82 78	118	172	228 212	255 237	232 216	178 165	123	82	62	51	46	45	46	52	63	84	121	175	229	250	221	163
49	57	74	104	149	197	220	200	154	108	77	59	50	46	45	47	53	66	89	129	188	246	269	238	175
47	55	70	78	140	184	204	186	143	101	73	57	49	45	45	48	55	68	94	137	200	264	288	255	187
46	53	67	93	131	172	196	173	133	95	69	55	48	45	45	48	56	71	96	145 154	213	281 299	308 327	272 288	199 210
44	51 49	64 62	88 84	124 118	162 154	179 170	163 155	125 119	90 86	66 64	53 5 2	47 46	44 44	45 45	49 50	58 59	74 77	103 108	162	239	316	345	304	222
43 42	48	60	81	114	148	163	148	115	83	62	50	45	44	46	51	61	79	113	169	251	332	362	319	232
41	47	58	79	110	143	158	144	111	80	60	50	45	44	46	52	62	B 2	117	176	261	346	378	332	242
40	46	57	77	107	139	154	140	108	79	59	49	45	44	46	52	64	84	120	182	271	359	392	344	250
39	45	56	75	105	137	151	137	106	77	58	49	44	44 44	. 47	53 53	65 66	86 87	123 126	167 192	279 286	370 378	404 413	355 362	257 262
38 38	44 43	55 54	74 74	104 103	135 134	149 148	135 135	105	76 76	58 58	48 48	44 44	44	47 47	54	66	88	128	195	290	383	418	366	265
37	43	54	73	103	133	147	134	104	76	58	48	44	44	47	54	67	89	129	197	292	385	419	367	265
37	43	54	73	103	134	148	134	104	76	5 B	48	44	44	47	54	67	90	130	197	292	383	416	364	263
37	43	54	73	103	134	148	L35	105	76	58	48	45	44	48	54	67	90	130	197	289	379	410	358	259
37	43	54	74	104	136	150	137	106	77	58 59	49 49	45 45	45 45	48 48	55 55	67 67	90 90	130 130	196 194	286 281	372 363	401 390	350 339	253 246
37 37	43 43	55 55	75 76	106	138 141	153 156	139	108	78 79	60	50	45	45	48	54	67	90	129	191	275	352	376	326	237
37	44	56	76	111	145	161	146	113	81	61	50	46	45	48	54	67	89	128	188	268	339	360	312	226
38	45	58	81	115	150	167	151	116	84	62	51	46	45	48	54	67	89	126	185	260	326	344	297	216
38	46	60	84	119	157	173	157	121	86	64	52	47	46	48	54	66	86	125	182	253	313	328	282	205
39	47	62	87	125	164	181 190	164 171	125	89 92	65 67	53 54	47 48	46 47	48 49	54 55	66 67	88 88	125	180	246 240	301 290	312 297	268 253	195 184
40 41	49 50	65 67	92 96	132 138	172 181	190	179	136	96	69	55	49	47	49	55	67	89	125	177	236	280	283	240	174
42	52	70	101	145	189	208	187	142	99	72	57	50	48	49	55	67	89	126	177	232	270	270	227	165
								F	'igu	ce A	-6.	(Sh	eet	5 of	6)									

Figure A-6. (Sheet 5 of 6)

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ECHELLOGRAM SUBSECTION	
TAPE 1107 - DESTRUCTIVE R/O SIMULATION(COMPLETE SYSTEM), LAMBOA = 1216 ANGST,	SEC PSF WIDTH = 41 MICRONS

	rs: ECS:	201 125						(ELS =		164 SL	JM = 0	.1093	SE 08											
									40	E 2	63	87	136	221	333	428	445	375	265	170	108	73	56	48
498	519	435	306	194	121	81 80	61 60	52 51	49 49	53 53	64	87	140	227	344	4 42	460	386	272	173	109	74	56	47
496	515	431	302 295	191 187	120	79	60	51	49	53	65	90	142	231	351	450	468	392	275	174	110	74	55	47
486	505 488	422 407	285	180	114	77	59	50	49	53	65	90	142	232	352	4 52	469	392	274	173	109	73	55	46
470 450	466	389	272	173	109	74	57	49	48	52	64	89	141	230	348	446	462	386	270	170	107	72	54	45
426	441	368	258	164	104	71	55	48	47	51	63	88	138	225	340	435	450	375	262	166	104	7C	53	44
400	414	346	242	154	99	68	53	47	46	50	61	85	134	217	328	420	434	361	252	160	101 97	68 66	51 50	43 42
373	386	322	226	144	93	65	51	45	44	49	59	8.2	120	208	313	400	413	344 324	241 227	153 145	92	63	48	41
345	356	297	209	134	87	61	49	43	43	47	57	79	122	196	295	376 350	389 361	302	212	136	87	60	47	40
316	325	271	191	123	81	58	46	42	41	45	55	75	115 107	184 170	275 254	322	333	278	196	126	82	57	45	39
286	295	245	174	113	75	54	44	40	40	43 41	52 49	71 66	100	157	233	295	304	254	180	117	76	54	43	38
Z 58	266	222	158	103	69	51 47	42 39	38 36	38 36	39	47	62	93	145	213	270	278	233	145	108	72	52	41	36
231	238	200	142	94 85	64 59	44	37	34	34	37	44	59	86	134	196	247	254	213	152	100	67	49	40	36
207 184	212 189	178 159	128 114	77	54	41	35	33	33	36	42	55	81	124	181	2 27	234	197	141	93	63	47	38	35
165	169	142	103	70	49	3.8	33	31	31	34	40	52	76	115	168	211	217	182	131	87	60	45	37	34
150	153	129	93	64	46	36	32	30	30	33	38	49	71	108	157	196	202	169	151	81	56	43	36 35	34 33
138	142	118	48	59	43	34	30	29	29	31	37	47	67	102	147	184	188	158	113	76 72	53 51	41 40	35	33
128	130	110	80	55	40	33	29	28	28	30	35	45	64	96	138	173	177	148 140	106 101	68	49	39	34	33
120	122	103	75	52	38	31	28	27	27	29	34	43	61 59	91 88	131 126	164 156	167 160	134	96	66	47	38	34	33
114	116	98	72	50	37	30	27	26	26	28 28	33 32	41 40	57	84	121	150	154	129	93	64	46	37	34	33
110	112	94	69	48	36	29	26	25 25	26 25	27	31	39	55	82	117	145	149	125	90	62	45	37	34	34
107	109	92	67	47 47	35 35	2 9 28	26 26	25	25	27	30	38	53	79	113	141	144	121	88	61	45	37	34	34
106	108 107	91 90	67 66	46	34	28	25	24	25	26	30	37	52	77	110	137	140	117	85	59	44	37	35	35
105 105	107	90	66	46	34	28	25	24	24	26	30	37	51	75	107	133	136	114	83	59	44	37	35	36
105	107	95	66	46	34	28	25	24	24	26	29	36	50	74	104	129	132	115	82	58	44	37	36	37
106	108	91	66	47	34	28	25	24	24	26	29	36	50	73	103	127	130	110	81	58	44	38 38	36 37	38 39
107	109	92	67	47	35	29	26	24	24	26	29	36	49	72	102	126	129	109	81 81	58 58	44 45	39	38	40
109	111	94	69	48	36	29	26	25	25	26	29	36	50 50	72 73	102	126 128	130 131	111	62	59	46	40	39	42
112	114	96	71	49	36	30	26	25	25	26	30 30	37 37	51	75	105	131	134	114	84	60	47	41	40	43
117	119	100	73	51	38 39	30 31	27 28	25 26	25 26	27 27	31	38	52	76	108	134	137	116	86	62	48	42	41	44
123	125	105	77 82	54 57	41	33	29	27	27	28	32	39	53	78	111	137	141	120	88	63	49	43	42	45
131 141	133 144	121	88	60	43	34	30	28	27	29	32	40	55	81	115	142	146	124	92	65	50	44	43	46
155	158	132	96	65	46	36	31	29	28	30	33	41	57	84	120	149	153	129	95	67	52	45	44	48 49
171	174	146	104	70	49	38	32	30	29	31	35	43	60	88	126	156	160	135	99	70	53	46 47	45 46	49
189	193	161	115	76	53	40	34	31	30	32	36	45	63	93	132	165	169	143 151	104	73 77	55 57	49	47	50
210	214	178	L26	83	56	42	35	32	32	33	38	47	66	98 105	141 151	175 187	179 192	161	117	81	60	50	48	51
233	237	196	138	90	61	45	37	34	33	34	39 41	50 53	70 75	113	162	201	206	172	124	85	62	52	49	51
259	262	216	151	98	65 69	48 50	39 41	35 36	34 35	36 37	43	56	Βĺ	122	175	217	221	184	132	89	65	53	50	52
233	287	237	165	106 114	74	53	43	38	37	39	45	59	86	131	180	233	237	197	140	94	67	54	50	52
308 334	313 339	257 278	178 192	121	78	56	44	39	38	40	47	62	91	139	201	249	253	210	149	99	70	56	51	53
358	363	293	205	129	82	58	46	41	39	42	49	65	96	148	213	265	270	223	157	104	72	57	52	53
381	386	315	216	135	86	60	48	42	40	43	51	68	101	155	225	280	285	235	165	108	74	58	52	53
401	406	331	-	141	89	62	49	43	41	44	52	70	105	163	236		299	247	172	112	77	59	53 63	53 53
417	422	344	235	146	92	64	50	44	42	45	54	73	109	170	247	307	312	257	179	116	78 80	60 61	53 53	52
428	433	353	240	149		65	51	44	43	46	55	75	113	176	256 263	31B 327	323 331	265 271	184 188	119 121	81	61	53	52
435	449	358	243	151	95	66	51	45	44	47	56 57	77 78	116	181 185	269	333	336	275	190	122	81	61	53	52
43B	442		244	151	95	66	52	45	44	47 48	5 f 5 8	79	110	187	271		339	277	191	122	82	61	53	52
435	438	356	242	150	95	56	52	45	44	40	70	, ,	ILV	101		,								

Figure A-7. Eschellogram Subsection - Tape No. 1107

		250	330	1.0	93	65	51	45	44	48	58	79	120	187	270	334	337	276	190	122	81	61	53	51	
429	431	350 340	238 232	148 144	92	64	51	45	44	47	57	79	119	185	267		333	272	188	120	80	60	52	51	
419	420	328	224	140	89	63	50	44	43	47	57	78	118	182	262	323	325	265	183	116	79	60	52	50	
406 390	406 388	314	214	134	86	61	49	44	43	46	56	77	116	179	255	313	315	257	178	115	77	59	51	50	
371	369	298	204	128	83	59	48	43	42	46	56	76	115	175	248	303	303	247	172	111	75	57	50	50	
352	348	281	193	122	79	57	47	42	41	45	55	76	113	171	241	292	29 L	237	164	107	73	56	50	49	
332	327	264	181	115	76	55	45	41	41	45	54	75	111	167	232	279	277	225	157	102	71	55	49	49	
312	306	246	169	109	72	53	44	40	40	44	54	73	109	162	223	266	262	213	149	98	68	54	48	49 49	
293	285	229	158	102	69	51	42	39	39	43	53	72	106	156	213	251	247	200	140	93	65	52	48 47	49	
275	265	213	147	96	65	49	41	38	38	42	52	71	103	150	202	237	231	187	132	68	63 60	51 50	47	49	
259	247	197	137	90	62	47	40	37	37	41	51	69	101	145	192	222	216	174	123	63		48	46	49	
245	231	184	128	85	59	45	39	36	37	41	50	68	98		183	209	200	162	114	78 74	58 55	47	46	50	
233	217	172	120	80	56	44	38	35	36	40	49	67	97		174		186	149 138	106 99	69	53	46	46	50	
223	205	161	112	75	54	42	37	35	35	39	49	67	95	132	166 159	183 172	172 159	127	92	65	51	45	45	50	
214	194	152	10.6	72	52	41	36	34	35	39	48	66	94 93	128 125	152	161	148	117	85	62	49	44	45	51	
208	186	144	101	69	50	40	35	34	34	39	48	66 65	92	122	145	152	137	109	79	58	47	43	45	51	
205	187	138	97	66	49	39	35	33	34 34	38 38	48 48	65	91	120	141	144	129	102	75	56	46	43	44	51	
205	177	135	94	65	48	39	34	33 33	34	38	48	66	92	119	138	139	122	96	71	54	45	42	44	51	
207	176	132	92	64	47	38 38	34 34	33	34	39	49	67	94	121	138	137	119	93	68	52	44	42	44	51	
212	177	131	91	63	47	38	34	33	35	39	50	69	97	125	141	137	117	90	66	51	43	41	44	51	
219	179	131	90 90	63 63	47 47	39	35	33	35	40	50	70	97	125	141	137	117	90	67	51	43	41	44	51	
219	179	131	91) 91	63	47.	39	35	34	35	41	52	73	102	130	145	139	116	89	65	50	43	41	44	51	
228 240	184 193	133 135	92	64	48	39	35	34	36	42	54	76	107	137	151	142	117	8.8	64	49	42	41	44	51	
256	199	140	94	65	49	40	36	35	37	43	56	80	113	145	157	146	118	88	64	49	42	41	43	51	
275	210	145	97	67	50	41	37	36	38	45	59	85	121	154	166	151	120	88	64	49	42	40	43	50	
296	223	152	100	69	51	42	38	37	39	47	62	91	129	164	176	158	124	89	64	49	42	40	43	50	
319	237	160	104	71	52	43	39	3.8	41	49	66	97	139	176	187	166	128	91	65	49	42	40	42	49	
342	251	167	108	73	54	44	40	39	42	5 I	70	103	149	189	200	176	133	93	66	49	42	40 40	42 41	48 47	
366	266	174	112	75	55	45	41	40	43	53	74	110	159	202	213	186	139	96	67	50 50	42 42	39	41	46	
390	280	182	116	77	57	46	42	41	45	55	78	117	170	216	227	196	145	99	68 69	51	42	39	40	45	
413	2 94	190	120	79	58	47	43	42	46	57	BI	124	182	230	241	207	151	102 105	71	52	42	39	39	44	
434	307	196	123	81	59	48	43	43	47	59	85	131	192	244	254 266	217 226	158 164	108	72	52	42	39	39	43	
45 L	318	202	126	83	60	49	44	44	48	61	88 91	137 142	201 209	256 266	277	235	169	111	73	53	42	38	38	41	
463	325	206	128	84	61	49	44	44	49	63	94	146	217	276	287	242	173	113	74	53	42	38	37	40	
469	328	207	128	84	6 L	50	45	45	50 50	64 65	96	150	223	283	294	247	176	114	74	53	42	37	36	39	
469	328	206	128	84	61	50 50	45 45	45 45	50 51	65	97	152	226	288	298	250	177	114	74	52	41	37	36	38	
464	3 2 4	203	126	83	61 60	49	45	45	50	65	97	153	228	290	299	250	176	113	73	51	41	36	35	37	
455	317	200	124	82	59	48	44	44	50	65	97	152	226	288	297	247	173	111	72	51	40	35	34	35	
442 427	309 2 98	194 198	121	80 78	58	47	43	44	49	64	95	150	223	282	291	242	170	109	70	50	39	34	33	34	
409	286	182	113	75	56	46	42	43	48	63	93	146	216	274	282	235	165	106	69	48	38	34	32	33	
389	272	172	108	73	54	45	41	42	47	61	90	141	208	264	272	226	159	102	67	47	37	33	31	32	
368	257	163	103	70	52	44	40	41	46	59	87	135	199	252	259	216	152	98	64	46	36	32	30	31	
346	242	153	97	66	50	42	39	39	44	57	83	129	189	239	247	206	145	94	62	44	35	31	30	31	
323	226	144	92	63	48	41	38	38	43	55	79	122	179	226	233	195	138	90	59	43	34	30	29	30 29	
301	2 10	134	86	60	46	39	36	37	4 L	52	75	115	169	213	219	184	130	85	57	41	33	29 29	28 28	29	
279	195	125	81	56	44	37	35	35	39	50	71	108	158	199	205	172	122	80	54 50	39 37	32 31	28	27	28	
258	181	116	76	53	42	36	33	34	38	47	67	101	147	185	190	159	113 104	75 69	90 47	35	29	27	26	28	
238	168	108	71	50	40	34	32	32	36	44	62	94	135	169	174 158	145 132	94	63	44	33	28	26	26	27	
220	155	101	66	48	38	33	31	31	34	42	58	86 79	124	154 139	142	119	85	57	41	32	27	25	25	27	
20.3	144	93	62	45	36	31	29	30	32	39 37	54 50	72	102	126	128	107	77	53	38	30	26	25	25	27	
189	133	87	58	42	34	30	28 27	28 27	31 29	35	46	46	93	114	116	97	70	49	36	29	26	24	25	27	
177	124	81	55	40	33	29			28	33	43	61	85	104	105	89	65	45	34	28	25	24	25	27	
167	117	77	52	39 37	32 30	28 27	26 25	26 25	27	31	41	57	78	95	97	82	60	43	32	27	24	24	25	27	
159	112	73 71	50 48	3 f	30	26	25	25	26	30	39	54	73	89	91	77	57	41	31	26	24	24	25	27	
152	107	71 68	48 46	35	29	26	24	24	25	29	37	51	69	84	86	73	54	39	30	26	24	24	25	27	
146 142	103	66	45	34	28	25	24	23	25	28	36	49	67	81	8.2	70	52	38	29	25	24	24	25	28	
138	98	54	44	33	28	25	23	23	24	28	35	48	65	79	80	68	51	37	29	25	24	24	25	29	
134	95	63	43	33	27	24	23	23	24	27	34	47	64	78	79	67	51	37	29	25	24	24	26	29	
132	93	62	43		27	24	23	23	24	27	34	47	64	77	79	67	50	37	29	25	24	24	26	30	
130	92	61	42	3.2	27	24	23	23	24	27	34	47	64	77	79	67	51	37	29	25	24	25	27	31	
129	92	61	42		27	24	23	23	24	27	34	47	64	78	79	68	51	37	29	26	24	25	27 28	31 32	
13C	92	62			27	24	23	23	24	27	35	48	65	79	81	69	52	38 38	30 30	26 26	25 25	25 26	28	33	
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Figure A-7 (Sheet 2 of 6)

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Figure A-7 (Sheet 3 of 6)

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ECHELLOGRAM SUBSECTION

TARE 1107 - DESTRUCTIVE RAD SIMULATION COMPLETE SYSTEM	. LANDOA = 1216 ANGST.	SEC PSF WIDTH = 41 MICRONS

	TS:	226		50						864 \$	UM =	0.109	3E 08											
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45	47	55	73	109	170	251	317	326	272	191	124	81	57	45	40	38	40	47	63	95	146	207 222	245 263	230 248
44	46	53	70	102	159	233	294	302	252	178	116	76	55	44	39	38 38	40 41	49 50	66 69	101 106	156 166	237	281	264
44	45	51	66	96	148	216	272 253	280 260	234 217	166 154	108 101	72 68	52 50	43 41	38 38	38	42	51	72	112	176	251	297	279
43	44	49 48	63 60	91 86	139 130	202 189	236	242	202	144	95	65	48	40	37	38	42	53	75	116	183	261	310	290
42 41	42 41	46	58	82	123	179	222	227	190	135	89	61	46	39	37	38	42	53	76	119	188	269	319	298
40	40	45	56	78	118	169	211	216	180	128	85	59	45	38	36	37	42	54	77	121	192	274	324	303
39	39	44	54	76	113	163	202	207	172	123	82	57	44	38	36	37	43	54	78	122	193	275	326	305
38	38	43	53	74	110	158	196	201	167	119	80	56	43	37	36	37	42	54	78	122	192	274	325	304
37	38	42	52	73	108	155	193	197	165	117	7 B	55	43	37	35	37	42	54	78	121	191	272 269	322 317	301 297
36	37	41	52	72	108	154	192	197	164	117	78 78	54 54	42 42	37 37	35 35	37 37	42 42	54 54	77 76	120 119	189 186	265	312	292
36	37	41	51	72	108	155 156	193 195	197 200	165 166	117 118	79	55	42	37	35	37	42	53	76	118	184	260	306	286
35 34	36 36	41 41	51 52	72 73	109	159	198	203	169	120	80	55	43	37	35	37	42	53	75	117	181	256	300	280
34	36	41	52	74	112	162	203	208	173	123	ВL	56	43	37	36	37	42	53	75	116	179	251	294	274
34	36	41	53	76	115	167	209	214	178	126	83	57	44	38	36	37	42	53	75	115	177	247	287	266
33	36	42	54	78	119	172	215	220	183	130	86	59	45	38	36	37	42	53	75	115	175	241	278	258
33	36	43	55	80	123	178	223	228	190	134	88	60	46	39	37	37	42	53	75	113	171	234	268	247
34	37	44	57	83	128	185	232	237	197	139	92	62	47	40	37	38	42	53	74	111	167	226	257	236
34	38	45	60	88	134	195	243	249	207	146	95	65	49	41	38	38	42	52	73 72	109 107	162 157	217 207	245 232	224 211
35	39	47	63	93	143	207	258	263	218	153	100	68	50 52	42 43	38 39	38 39	42 43	52 52	72	106	152	199	220	199
3.5	47	49	66	99	153 164	221 238	275 295	280 301	232 248	163 174	106 113	71 75	55	45	40	40	43	53	72	105	149	191	209	188
36 37	41 43	51 54	71 75	196 114	177	257	319	324	268	187	120	79	58	47	41	41	44	53	73	104	146	185	199	177
38	45	57	B1	123	192	279	347	352	290	202	129	85	61	48	43	42	45	54	73	104	144	179	191	168
40	47	61	87	133	209	304	378	383	315	219	139	90	64	51	44	43	45	55	74	105	143	175	183	160
41	49	65	93	144	227	331	412	418	344	238	150	97	68	53	46	44	47	56	75	106	143	172	177	153
43	52	68	100	156	247	362	451	457	375	258	162	103	72	56	48	45	48	58	77	108	144	170	172	147
44	54	73	107	109	269	394	491	498	408	280	175	110	76	58	50	47	49	59	80	111	146	170 172	169 158	142 139
46	57	7.7	114	181	290	427	533	540	442	302	188	117 125	80 84	61 64	52 54	49 50	51 53	62 65	84 88	116 123	151 158	178	170	138
48	60	81	121	194 296	31 <i>2</i> 333	460 492	575 615	583 623	475 508	324 346	200 213	132	88	67	56	52	56	68	93	130	167	185	174	139
50 51	62 65	85 39	134	218	353	522	653	662	538	365	224	138	92	69	58	54	58	72	99	139	178	195	180	142
53	67	92	141	229	371	550	688	696	566	384	235	144	96	72	60	56	61	76	106	149	190	206	187	145
54	69	96	140	238	388	574	719	727	590	399	244	149	99	74	62	58	63	80	113	160	203	218	196	149
56	71	98	151	246	401	595	744	752	610	412	251	153	102	76	64	60	66	85	121	172	218	232	205	155
57	72	101	154	253	412	610	763	771	625	421	256	156	104	77	65	62	69	90	129	185	234	247	216	160
58	73	102	157	258	419	620	775	782	633	427	259	158	105	78 79	56	64	72 74	94 99	138 146	198 211	250 266	263 278	227	166 171
58	74	103	159	260	423	624	77 9 775	785 780	635 631	428 425	260 258	159 158	105 105	79	67 68	65 67	77	104	154	223	282	292	247	177
59 59	75 75	104 104	160 159	261 259	422 419	622 615	763	767	620	417	254	156	105	79	69	68	79	108	162	235	296	306	257	182
60	75	134	15B	257	412	603	745	748	604	407	248	153	103	79	69	69	8í	112	169	246	311	320	266	187
60	74	103	157	253	404	586	722	722	582	393	240	149	101	78	68	69	83	115	176	257	324	333	275	191
59	74	102	155	248	393	566	693	691	557	376	231	144	99	77	68	70	84	119	182	267	337	345	284	196
59	73	101	152	242	380	544	661	657	529	357	221	13B	96	75	67	70	85	121	187	276	348	355	291	199
59	73	99	149	236	367	520	628	621	499	338	209	132	92	73	66	69	85	123	191	282	355	362	295	201
58	72	98	146	230	354	496	594	584	469	318	198	126	89	71	65	68 67	85 84	123 122	192 192	285 284	359 358	365 363	297 295	202 199
58	71	96	144	224	342	472	560 524	547	438	297 277	186 174	119 113	85 81	69 66	63 62	66	82	120	188	279	352	356	288	195
57 57	70 69	95 94	141	219 214	329 317	449 426	526 494	511 475	408 378	257	163	106	77	64	60	64	80	117	183	271	341	345	279	188
56	68	93	137	209	307	406	463	442	350	239	152	100	74	61	58	62	78	113	176	259	326	329	266	180
56	68	92	136	206	298	388		412	325	222	142	95	70	59	55	60	75	108	167	246	308	311	251	170

Figure A-7 (Sheet 4 of 6)

	56 55	67 67	92	136 136	205 205	293 288	374 362	413 392	365 361	281	191	133 124	89 84	67 63	56 54	53 51	57 55	71 68	102 96 91	158 148 138.	231 215 200	289 268 249	291 271 251	235 219 204	159 149 139
	55 55	67 67	92 93	137 139	205 207	286 285	352 344	374 359	339 320	262 245	178 167	116 109	80 75	60 58	52 49	49 47	52 50	6 4 61	85	129	186	231	233	189	130
	55	6B	94	141	210	285	340	348	305	231	157	104	72	55	48	45	48	58	80	120	172	214	215	175	120
	55	68	96	144	214	288	338	339	293	220 210	149 142	98 94	69 66	53 51	46 44	43 42	46 44	55 52	75 70	111 104	159 148	197 182	199 183	162 149	112 103
	55 55	69 70	98 101	148 153	220 22 7	294 302	339 344	334 333	283 277	203	137	91	64	50	43	40	42	49	66	96	137	168	168	137	95
	56	72	104	160	237	314	352	335	274	198	133	88	62	49	42	39	40	47	62	90	126	155	155	126	87
	57 58	74 76	108 113	168 177	250 264	328 346	365 380	341 349	274 276	195 194	130 128	86 84	61 60	48 47	41 40	38 37	39 38	45 43	59 55	84 78	117	143 132	143 132	116 107	81 75
	59	79	118	186	219	364	397	360	279	193	126	83	59	46	39	36	36	41	52	73	101	123	123	100	70
	60	8 I	123	196	295	384	414	370	283	193	125	82	58	45	39	35	35	39	50 47	69 65	95 89	114 107	114	93 87	66 62
	61 62	84 86	129 134	206 215	310 325	493 421	431 448	381 391	286 290	193 193	124 123	8 Z 8 1	58 57	45 45	38 38	35 34	35 34	38 37	46	62	84	101	101	82	59
	63	89	138	224	339	438	464	401	294	193	123	80	57	44	37	34	33	36	44	59	80	96	96	79	56
	64	91	143	232	351	454	478	410	298	194	122	80	57	44 44	37 37	33 33	33 32	35 35	43 42	57 56	77 75	92 89	92 89	75 73	54 53
	65 65	93 94	146 149	239 244	362 370	467 477	490 499	418 424	300 302	194 194	122	79 79	56 56	43	37	33	32	34	41	55	74	88	88	72	52
	66	95	151	247	376	483	504	426	30 <i>2</i>	193	120	78	56	43	36	33	32	34	41	55	74	88	88	73	52
	66	95	152	249	378	486 486	506 506	426 426	30 L 30 L	191 191	119 119	77 78	55 55	43 43	36 36	33 33	32 32	34 34	42 42	56 56	75 75	90 90	90 90	74 74	53 53
	66 66	95 95	152 152	249 250	375 379	486	506	424	299	189	117	77	55	43	36	33	32	35	43	57	77	93	93	76	55
	66	95	152	249	377	485	5 C 3	421	295	187	116	76	54	42	36	33	32	35	43	59	80	97	97	79 82	56 58
	65 65	94 93	150 148	241 243	374 369	480 473	498 490	416 408	291 285	183 179	114	75 73	54 53	42 42	36 36	33 33	32 33	36 36	44 46	61 63	83 87	101	101	86	56 61
	64	91	146	238	361	462	478	398	278	175	109	72	52	41	35	33	33	37	47	66	90	110	110	90	63
	62	89	142	232	351	449	464	386	269	169	106	70	5 i	41 40	35 35	33 33	33 34	38 39	49 51	68 72	94 100	115 121	115 122	94 99	66 70
	61 59	87 84	138 133	225 216	339 326	434 416	44B 430	373 358	260 250	164 158	102 99	69 66	50 49	40	35	33	35	40	53	76	106	130	130	106	74
	5 A	81	128	707	311	398	411	342	239	152	96	64	48	39	35	34	36	42	56	81	114	140	140	114	80
,	56	78	122	197	296	377	390	325	228	145	92	62	47	39 38	35 35	34 35	37 36	44 47	60 65	88 96	124 136	153 167	153 168	124 136	86 93
	54 52	75 72	116 110	186 175	279 261	356 332	367 343	3 C 6 2 8 6	215 201	137 129	87 83	60 57	45 44	37	35	35	39	49	70	105	149	184	184	148	101
	50	68	103	164	244	309	319	266	187	120	78	55	43	37	35	36	41	53	76	115	164	201	201	161	110
	48	65	97	153	226	287	295	246 228	174 162	113	74 70	52 50	42 40	36 36	35 35	37 37	43 44	56 59	82 88	125 135	179 194	220 239	219 238	176 191	119 129
	46 44	61 53	91 86	143	210 195	265 246	273 253	212	150	98	66	48	39	36	35	38	46	62	94	145	210	260	259	207	139
	42	55	৪১	124	181	228	234	196	139	92	62	46	38	35	36	39	46	66	100	156	227	280	280	223	149
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	38	48	68	102	147	183	187	156	112	75	53	41	36	35	37	42	54	76	119	190	278	344	343	273	181
	37	46	65	97	139	173	177	148	106	71	51	40	36	35 35	37 38	43 44	56 57	80 84	126 132	201 211	294 310	365 384	363 382	288 303	191 200
	35 34	44 43	62 60	93 90	133 129	166	169 164	142 137	101 98	69 67	49 48	39 39	3.5 3.5	35	38	45	59	87	138	221	324	402	399	316	208
	34	42	59	87	125	155	159	133	96	65	47	38	35	35	38	46	61	89	142	229	337	418	415	329	216
	33 32	41 40	57 56	85 84	122	152 150	156 153	130 128	94 93	64 63	46 46	38 38	35 35	35 35	39 39	47 47	62 63	92 94	147 151	237 243	348 357	432 443	429 439	339 347	222 227
	32	40	56	83	119	149	152	127	92	63	46	38	35	35	39	48	64	96	154	248	364	450	445	351	230
	31	39	55	83	119	148	152	127	92	63	46	38	35	36	40	48	65	97 98	156 157	250 251	367 366	452 450	447 444	352 350	230 229
	31 31	39 39	55 55	83 83	119	148 149	152 152	127 128	92 92	63 63	46 46	38 38	35 35	36 36	40 40	48 49	65 66	98	157	250	363	444	438	344	225
	31	39	56	84	120	150	154	129	93	64	46	38	35	36	40	49	66	98	156	248	357	436	428	336	220
	31	40	56	85	122	153 157	157 161	131 135	95 97	65	47 47	38 39	35 35	36 36	40 40	49 49	66 66	98 98	156 154	245 240	350 341	424 411	415 400	326 313	213 205
	31 32	40 41	57 59	87 89	125 129	161	165	138	99	66 67	48	39	36	36	40	49	65	97	152	235	330	395	383	299	196
	32	42	61	92	134	167	171	143	103	69	49	40	36	36	40	49	65	97	150	230	319	378	364	284	187
	33 34	43 45	63 66	96 101	139 146	174 183	178 187	149 156	106	12 74	51 52	40 41	37 37	37 37	40 40	48 49	65 65	96 96	149 147	224 220	308 297	361 344	346 328	269 254	177 168
	35	47	69	106	154	192	196	163	115	77	54	42	38	37	40	49	65	96	147	216	288	329	311	240	158
	36	49	73	113	163	202	206	171	120	80	55	43	38	38	41	49	66	97	147	214	280	315	294	226	150
•	37 38	51 53	77 80	118 124	171 179	212 222	215 225	178 186	126 131	83 86	57 59	44 45	39 40	38 39	41 42	49 50	66 67	98 99	148 149	212 211	273 267	302 290	279 264	213 201	141 133
	40	55	83	129	187	232	235	194	136	89	61	47	40	39	42	51	69	101	151	211	262	280	251	190	126
	41	57	87	135	195	243	246	203 213	143 149	93 97	63 65	48 49	41 42	40 41	43 44	52 53	70 71	103 106	153	212 214	258 257	271 264	240 231	180 172	119
	42	59	90	141	204	254	258	413	144						5 of		• •	100	.,,	617	.,,	207		*14.	***

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45	64	99	155	226	282	287	236	164	106	70	53	45	43	47	57	79	118	173	230	263	256	213	154	101
47	67	103	163	238	297	302	248	172	110	73	54	46	44		-	82	123	161	239	270	258	210	150	99
48	69	108	171	251	312	317	260	180	115	76	56	47	45	48	59		129	190	250	279	262	210	148	97
50	72	113	179	262	326	33 L	27 L	187	119	78	57	48	46	50	61	86	137	202	263	290	268	212	148	96
52	75	117	186	272	339	343	281	193	122	80	59	49	47	51	64	90		215	279	304	277	215	148	96
53	77	121	192	280	349	353	288	198	125	82	60	50	48	53	66	95	145		296	320	287	220	149	96
54	78	123	195	286	356	360	294	202	127	83	61	51	50	55	69	100	154	228	314	337	299	225	151	97
54	79	124	197	289	359	363	296	203	1,28	84	62	52	51	56	72	105	163	243	333	355	312	232	154	98
55	8Ó	125	198	289	359	362	296	203	128	84	62	53	52	58	75	110	173	257	351	373	324	239	157	99
55	60	125	197	287	356	358	292	201	127	84	62	53	53	60	78	116	182	272	369	390	337	245	160	100
56	80	125	196	283	350	352	287	197	125	83	62	54	54	61	80	121	191	286	386	406	348	251	162	101
56	80	124	194	278	342	343	279	192	123	82	62	54	54	62	83	125	200	300		421	359	256	164	102
56	80	123	191	272	332	332	271	187	120	81	61	54	55	64	85	130	208	312	402	434	367	261	166	103
56	80	122	188	265	323	322	262	181	117	79	61	54	55	64	87	134	215	323	415	445	375	264	167	103
57	80	122	185	259	313	311	253	175	113	77	60	54	55	65	89	137	221	332	427	453	380	266	167	103
57	81	122	183	254	304	300	244	169	110	75	59	53	55	66	90	139	225	339	435		383	268	167	103
58	82	123	103	250	296	290	234	163	106	73	58	53	55	66	90	141	228	344	441	458	384	267	167	102
58	83	124	102	246	287	279	225	156	103	71	57	52	55	66	91	141	229	346	444	460	382	265	165	101
59	84	125	182	241	278	268	215	149	99	69	55	51	54	65	90	141	229	346	443	459	377	261	162	99
60	85	126	181	237	269	257	205	143	95	67	54	50	54	65	89	140	227	343	439	454		255	158	97
61	87	128	181	233	261	248	196	136	91	65	53	50	53	64	88	137	223	337	431	445	369	248	154	95
62	89	136	183	231	254	237	187	130	87	63	52	48	52	62	86	134	217	328	419	432	359	_	-	92
64	91	133	184	229	248	228	179	124	84	61	50	47	50	61	84	130	210	317	404	417	346	239	149 143	89
65	93	136	187	228	242	220	171	119	81	59	49	46	49	59	81	125	202	303	387	399	331	230		85
67	96	140	190	228	238	212	164	114	78	57	48	45	48	57	78	120	193	289	368	380	315	219	137	
69	99	144	194	229	234	206	158	110	75	56	46	44	47	55	75	114	183	273	347	358	298	207	130	81
-	193	149	199	232	233	201	153	106	73	54	45	43	45	53	72	108	172	257	326	336	279	194	122	76
71	107	155	206	237	234	199	149	103	71	53	44	42	44	51	68	102	161	240	304	313	260	181	114	72
73	113	165	217	245	237	198	147	101	70	52	44	41	42	49	65	96	151	223	282	290	241	168	106	67
77		175	229	257	244	200	146	100	69	51	43	40	41	47	61	90	140	20 a	260	267	222	155	39	63
BL	1.20		245	271	253	203	146	99	6 B	51	42	39	40	45	58	84	130	190	239	246	204	143	91	59
85	128	188	243	2/1	673	203	140	100	40	6.1	4.7	3.8	39	43	55	78	120	174	219	224	186	131	84	55

APPENDIX B

EXPANSION FORMULAE FOR HANKEL TRANSFORM OF TRUNCATED GAUSSIAN POINT SPREAD FUNCTION

B.1 INTRODUCTION

The calculation of the two-dimensional Fourier transform of an axially symmetric point spread function (PSF) may be reduced to the Hankel transform of the radial PSF. In this Appendix we derive an infinite series by partial integration for the case of a circular Gaussian profile truncated by a clear circular aperture. An alternative formula, which is obtained by interchanging the u and dv variables in the partial integration, is quoted from the literature (Reference 5). These formulae yield the well known results of the diffraction pattern of a clear circular aperture and the Gaussian MTF in the limiting cases of $r_0/\sigma <<1$ and $r_0/\sigma >>1$, respectively, where r_0 is the radius of the truncating aperture, and σ is the standard deviation of the Gaussian profile.

B.2 EVALUATION OF HANKEL TRANSFORM

We start with the Hankel transform expression,

$$M(s) = (1/\sigma^2) \int_{0}^{r_0} J_0(2\pi rs) \exp(-r^2/2\sigma^2) r dr,$$
 (B-1)

where J is the Bessel function of order zero, and s is spatial frequency. Letting $z=2\pi rs$ and $\delta=2\pi\sigma s$ the integral (B-1) becomes

$$M = (1/\delta^2) \int_0^{Z_0} J_0(z) \exp(-z^2/2\delta^2) z dz,$$
 (B-2)

where

$$z_o = 2\pi r_o s$$
.

We now integrate by parts, letting $u=J_0(z)$ and $dv=\exp(-z^2/2\delta^2)$ zdz, and using the relation (1/z)(d/dz) $(J_n(z)/z^n)=-J_{n+1}(z)/z^{n+1}$.

Thus

$$M = -J_0(z)\exp(-z^2/2^2)$$
 $\Big|_0^{z_0} - \int_0^{z_0} (J_1(z)/z)\exp(-z^2/2\delta^2) zdz.$

Integrating by parts again gives

$$M = -J_{o}(z)\exp(-z^{2}/2\delta^{2}) \mid {z \choose 0} + \delta^{2}(J_{1}(z)/z)\exp(-z^{2}/2\delta^{2}) \mid {z \choose 0}$$

$$+ \delta^{2} \int {z \choose 0} (J_{2}(z)/z^{2})\exp(-z^{2}/2\delta^{2}) zdz.$$

Continuing this process and evaluating the upper and lower limits of integration with the help of the limit: $\lim_{n \to \infty} (J_n(z)/z^n) = (1/2^n n!)$ we get the infinite series

$$M = 1 - J_{o}(z) \exp(-z_{o}^{2}/2\sigma^{2}) - \delta^{2}[1/2 - (J_{1}(z_{o})/z_{o}) \exp(-z_{o}^{2}/2\sigma^{2})]$$

$$+ \delta^{4}[1/2^{2}2! - (J_{2}(z_{o})/z_{o}^{2}) \exp(-z_{o}^{2}/2\sigma^{2})]$$

$$- \delta^{6}[1/2^{3}3! - (J_{3}(z_{o})/z_{o}^{3}) \exp(-z_{o}^{2}/2\sigma^{2})]$$

$$+ \dots$$

which can be separated into the sum of two infinite series:

$$M = 1 - \delta^{2}/2 + (1/2!) (\delta^{2}/2)^{2} - (1/3!) (\delta^{2}/2)^{3} + \dots$$

$$-\exp(-z_{o}^{2}/2\sigma^{2}) \left[J_{o}(z) - \delta^{2}J_{1}(z_{o})/z_{o} + \delta^{4}J_{2}(z_{o})/z_{o}^{2} + \delta^{4}J_{2}(z_{o})/z_{o}^{2}\right]$$

$$+ \delta^{3}J_{3}(z_{o})/z_{o}^{3} - \dots$$

The first series is recognizable as the expansion of $\exp(-\delta^2/2)$; hence the expansion formula of the Hankel transform is written, finally, as

$$M(s) = \exp(-2\pi^{2}\sigma^{2}s^{2})$$

$$-\exp(-r_{o}^{2}/2\sigma^{2}) \sum_{n=0}^{\infty} (-4\pi^{2}\sigma^{2}s^{2})^{n} J_{n} (2\pi r_{o}^{s})/(2\pi r_{o}^{s})^{n}, \qquad (B-3)$$

where \mathbf{z}_{0} and δ have been replaced by their corresponding parameters.

In the limit $r_0/\sigma >> 1$, (B-3) clearly reduces to the MTF of a Gaussian PSF. It is evident that the series diverges for any fixed r_0/σ for s large enough. Hence, the usefulness of the formula is limited to the region $2\pi\sigma s/(r_0/\sigma) < 1$.

B.3 ALTERNATIVE FORMULA FOR THE REGION $2\pi\sigma s/(r_0/\sigma) > 1$

In Reference 5 a similar calculation is performed with the u and dv interchanged in the partial integration. The result in our notation is

$$M(s) = \frac{(r_{o}/\sigma)^{2}}{\exp(r_{o}^{2}/2\sigma^{2})-1} \sum_{n=o}^{\infty} \frac{2n}{(r_{o}/\sigma)} J_{n+1}(2\pi r_{o}^{s})/(2\pi r_{o}^{s})^{n+1}, \quad (B-4)$$

which reduces in the limit $r_0/\sigma < 1$ to

 $M(s) \cong 2\ J_1^{(2\pi r_o s)/(2\pi r_o s)}, \ \text{which is the well-known Fraunhofer diffraction}$ pattern for a clear circular aperture illuminated by an incoherent plane wave. It is evident that this series converges only in the region $2\pi\sigma s/(r_o/\sigma) \ge 1, \ \text{so that the two formulae (B-3) and (B-4) are complementary.}$

B.4 COMMENT

In practice, the two expansion formulae may provide an aid in analysis, but in numerical computations involving the use of a computer it is probably faster and more accurate to perform a direct numerical integration of (B-1) using the polynomial approximation to the Bessel function J_0 and Simpson's rule, which was ultimately done in this study. An attempt to numerically evaluate (B-3) on the computer using an IBM Scientific Software Package

subroutine for the J ran into difficulty since the subroutine apparently is not accurate for the small argument region of the J , i.e., in the region $2\pi r_0 s <<1$.